INFORMATION TO USERS

This was produced from a copy of a document sent to us for microfilming. While the most advanced technological means to photograph and reproduce this document have been used, the quality is heavily dependent upon the quality of the material submitted.

The following explanation of techniques is provided to help you understand markings or notations which may appear on this reproduction.

- 1. The sign or "target" for pages apparently lacking from the document photographed is "Missing Page(s)". If it was possible to obtain the missing page(s) or section, they are spliced into the film along with adjacent pages. This may have necessitated cutting through an image and duplicating adjacent pages to assure you of complete continuity.
- 2. When an image on the film is obliterated with a round black mark it is an indication that the film inspector noticed either blurred copy because of movement during exposure, or duplicate copy. Unless we meant to delete copyrighted materials that should not have been filmed, you will find a good image of the page in the adjacent frame.
- 3. When a map, drawing or chart, etc., is part of the material being photographed the photographer has followed a definite method in "sectioning" the material. It is customary to begin filming at the upper left hand corner of a large sheet and to continue from left to right in equal sections with small overlaps. If necessary, sectioning is continued again—beginning below the first row and continuing on until complete.
- 4. For any illustrations that cannot be reproduced satisfactorily by xerography, photographic prints can be purchased at additional cost and tipped into your xerographic copy. Requests can be made to our Dissertations Customer Services Department.
- 5. Some pages in any document may have indistinct print. In all cases we have filmed the best available copy.

University
Microfilms
International

300 N. ZEEB ROAD, ANN ARBOR, MI 48106 18 BEDFORD ROW, LONDON WC1R 4EJ, ENGLAND

7921245

LEE, JIM CLYDE A COST-EFFECTIVENESS EVALUATION OF A DIGITAL COMPUTERIZED TRAFFIC SIGNAL SYSTEM.

THE UNIVERSITY OF OKLAHONA, PH.D., 1979

University
Microfilms
International 300 N. ZEEB ROAD, ANN ARBOR, MI 48106

THE UNIVERSITY OF OKLAHOMA GRADUATE COLLEGE

A COST-EFFECTIVENESS EVALUATION OF A DIGITAL COMPUTERIZED TRAFFIC SIGNAL SYSTEM

A DISSERTATION

SUBMITTED TO THE GRADUATE FACULTY

in partial fulfillment of the requirements for the

degree of

DOCTOR OF PHILOSOPHY

ΒY

JIM CLYDE LEE

Norman, Oklahoma

1979

A COST-EFFECTIVENESS EVALUATION OF A DIGITAL COMPUTERIZED TRAFFIC SIGNAL SYSTEM

APPROVED BY

DISSERTATION COMMITTEE

Acknowledgements

The author would like to express appreciation to the dissertation committee for their assistance in this effort. Particular appreciation is due Dr. J. G. Laguros and Dr. Allen R. Cook, both of the School of Civil Engineering and Environmental Science of the University of Oklahoma, for their guidance, suggestions and constructive criticism of this paper.

Additionally gratitude is due the City of Amarillo Traffic Engineering Department and, in particular, Richard H. Davis for assistance in obtaining portions of the data for this study.

The author is also indebted to the Federal Highway Administration of the U.S. Department of Transportation for a Highway Safety

Fellowship in the academic year 1974-75 which assisted financially in this pursuit of graduate study at the University of Oklahoma.

Gratitude is also expressed to the author's wife, Susan, for her assistance in data reduction, draft typing and, most importantly, encouragement in this lengthy process.

Abstract

In this dissertation a digital computerized traffic signal system controlling 133 intersections in Amarillo, Texas is evaluated. The evaluation is performed in the form of a before-after study which compares the number of stops, amount of delay and number of accidents occurring in the period prior to as well as after installation of the computer traffic signal system. The stop and delay data are obtained with travel time and studies using the average car method. The stop delay and accident data are summarized for the individual studies of the section. This includes both a downtown grid section and a series of arterials. Several different methods of control which were used prior to installation of the computerized system are discussed and compared with the new system. An analysis is also included estimating the reduction in air pollutants as a result of the improved traffic operation.

The main objective of this research is to compare the reduction and road user cost in the form of reduced stops and delay with the increased cost of installation and operation of the computerized traffic signal system. This cost effectiveness operation is performed using both a benefit cost ratio and a rate of return method of analysis.

TABLE OF CONTENTS

| | Pa | ıge |
|----------------|---|----------------------------|
| LIST | OF TABLES | ii |
| LIST | OF ILLUSTRATIONS | ii |
| Chapt | er | |
| I. | INTRODUCTION | 1 |
| II. | DESCRIPTION OF COMPUTERIZED SIGNAL SYSTEM | |
| | | 11 12 |
| III. | EXPERIMENTAL DESIGN, DATA COLLECTION AND ANALYSIS METHODOLOGY | |
| | | 14 19 20 21 23 |
| IV. | ANALYSIS | 24 |
| V. | RESULTS | 41 |
| VI. | CONCLUSIONS | 51 |
| BIBLI | OGRAPHY | 54 |
| Apper | dices | |
| A. B. C. | Travel Time Data | 5 <i>6</i> |
| | Individual Street and Direction | 66 |
| D. | t-Test Evaluation of Number of Stops in Entire System | 97 |
| E. | Chi Square Evaluation of Number of Stops | .02 |
| F. | Computation of Decay Per Day | |
| G. | t-Test Evaluation of Decay in Entire System | |

| | | Pag |
|----|---|------|
| н. | t-Test Evaluation of Number of Stops by Section | . 11 |
| I. | Calculation of Vehicle Operating Costs | . 12 |
| J. | Fuel Consumption Reduction Worksheet | · 12 |
| K. | Air Pollution Reduction Worksheet | - 12 |

LIST OF TABLES

| TABLE | | Page |
|-------|--|------|
| 1. | Operational Improvements of Selected Systems | 2 |
| 2. | Installation Costs of Selected Systems | . 4 |
| 3. | Cost of Principal Items | . 8 |
| 4. | Adams Street-Northbound A.M. Peak | 26 |
| 5. | Before-After Comparison of Stops and Delay in Six Travel Time Runs During Each Time Period | 26 |
| 6. | Stop and Delay Comparison by Section • • • • • • • • • • • • • • • • • • • | 30 |
| 7. | Yearly Accidents by Section | 33 |
| 8. | Significance Tests of Accident Reduction | , 34 |
| 9. | Accident Summary | 35 |
| 10. | Comparison of Motorists' Operating Costs | , 48 |
| 11. | Impact of Amarillo Computerized Signal System | 49 |

LIST OF ILLUSTRATIONS

| FI | GURI | E |] | Page | • |
|----|------|--|---|------|---|
| | 1. | Amarillo Computerized Traffic Signal System | 4 | 6 | |
| | 2. | Significance Test for Reduction in Accidents | • | 22 | |
| | 3. | Significance Test for Reduction in Stops | • | 28 | |
| | 4. | t-Test Analysis of Reduction in Stops in the Entire System | • | 43 | |
| | 5. | t-Test Analysis of Reduction in Delay in the Entire System | _ | 45 | |

CHAPTER I

INTRODUCTION

Numerous cities across the country and around the world have installed or are in the process of installing a digital computer controlled traffic signal system. Although results of these installations have been favorable, there has been a limited amount of evaluation. Pignataro (1, p. 374) there has been a limited amount of evaluation. Pignataro (1, p. 374) there is a "definite trend" toward these systems. Due to the relatively large capital and operating expenses of such systems it is believed that a cost effectiveness evaluation would be in order. It is the purpose of this research to measure the effectiveness of the system and to relate the cost of the system to the benefits the motorists derive from its operation.

Most cities which have installed computer controlled signal systems have engaged in some degree of system evaluation. Table 1 summarizes the results of some of these system evaluations as listed by Stockfish (2). These data are results of traffic operation before and after the installation of the computerized signal system.

Although these and other system evaluations indicate improvement, notably lacking is a comparison of the cost of the system with the

^{*} See References

TABLE 1
OPERATIONAL IMPROVEMENTS OF SELECTED SYSTEMS

| Cá tro | Number of | Percent Reduction | | | | | | | |
|---------------|---------------|-------------------|-------|-----------|-------------|--|--|--|--|
| City | Intersections | Delay | Stops | Accidents | Travel Time | | | | |
| Toronto | 864 | 20 | 53 | 13 | 44 | | | | |
| San Jose | 59 | 12 | 7 | NA | NA | | | | |
| Wichita Falls | 77 | 18 | 8 | 9 | NA | | | | |
| New York | 433 | 30 | 30 | NA | 20-40 | | | | |
| West London | 100 | 18 | NA | 18 | 9 | | | | |

value to the motorists in terms of reduced cost due to reduced travel time, fewer stops, fewer speed change cycles, etc.

A recent publication, <u>Traffic Control Systems Handbook</u>, (3, p. 612) reports costs of selected urban street traffic control systems as shown in Table 2.

In examining this table, the reader will find a wide range in system costs even when the number of intersections interfaced with the computer is considered. The main reason for this apparent discrepancy is the varying scope of the different projects. Some of the projects provided for all new local intersection equipment (poles, arms, signal heads and local controllers) while others required only the installation of the computer and peripheral equipment. Another factor in the wide variation in cost is the availability of conduit for communication of the computer to the local intersections. If existing conduit is available, a significant savings in the contract price can be realized. If conduit is not available, the contract may provide for aerial communication or leased telephone lines both of which result in a lower initial cost than the installation of underground conduit. Additionally, an initial savings might be realized by utilizing either time-division or frequency-division multiplexing both of which reduce the number of pairs of communication cable required for a given number of intersections.

The idea of a cost-effectiveness evaluation of improvements has been proposed for some time, notably by Winfrey (4). Its primary use has been in the evaluation of alternatives of construction and reconstruction of roadway facilities. This has been used in a limited way in the field of traffic control. Dudek and McCasland (5) utilized a cost-effectiveness

TABLE 2

INSTALLATION COSTS OF SELECTED SYSTEMS

| City | Date of Bid | Number of Intersections | Number of Detectors | System Bid Cost (in Dollars) |
|----------------------|-------------------|----------------------------|------------------------|------------------------------------|
| Charlotte, N.C. | | 174 | 55 | \$1,250,000 |
| Baltimore, Md. | | 900 | 1000 | 3,900,000 |
| Oklahoma City, Okla. | | 33 | | 133,572 |
| Shreveport, La. | | 256 | 500 | 762,000 |
| L.A. County, So. Bay | | 111 | | 645,000 |
| Denver, Colo. | | 320 | | 550,000 |
| Atlanta, Ga. | | 12 | | 169,000 |
| Savannah, Ga. | | 97 | 101 | 758,000 |
| Albany, Ga. | | 60 | 60 | 670,000 |
| Raleigh, N.C. | | 154 | | 661,000 |
| Pasadena, Tex. | | 63 | 75 | 145,820 |
| Phoenix, Ariz. | 1973 | 253 | 175 | 785,000 |
| Lansing, Mich. | 1974 | 150 | 155 | 649,000 |
| Tucson, Ariz. | 1974 | | | 528,000 |
| Amarillo, Texas | 1974 | 133 | 94 | 1,751,723 |
| Greensboro, N.C. | 1973 | 159 | 227 | |
| Columbus, Ohio | | 92 | 230 | |
| Laredo, Texas | 1973 | 65 | 40 | |

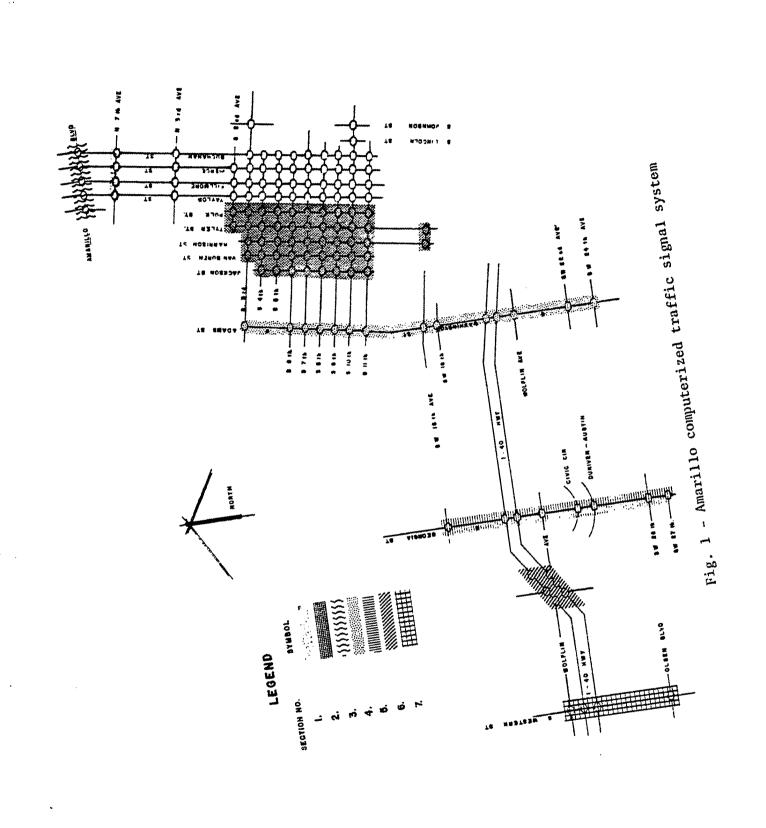
evaluation of alternatives of freeway merging control. In this study four levels of ramp merging control were evaluated. The implementation cost of each level was compared with the savings to the motorists in an attempt to optimize the effectiveness of ramp control with regard to its cost.

Another consideration in studies of improved signal systems should be the fuel savings that would be associated with the improvement. A test conducted at the General Motors Research Laboratory (6) showed that travel time per unit distance was the single most important factor in explaining the variability of fuel consumption. A method of computing the reduction in fuel savings has been developed to measure traffic engineering improvements in New York State (7). In the New York State method the additional fuel requirements are computed for idling while stopped and making additional stops as presented by Claffey in NCHRP Report 111 (8). The same type of analysis can be performed using the fuel consumption data for excess idling and stops presented by Winfrey (4).

The subject of this research is a new computer controlled traffic signal system which was installed in Amarillo, Texas in 1975 (9).

One hundred and thirty-three intersections were originally placed under computer control (Figure 1). These intersections vary from being a part of a tightly formed central business district grid network to those that comprise arterial street systems. Both one-way and two-way streets are involved. Figure 1 depicts the signal system with its seven sections.

Generally, a section is a group of intersections which were coordinated by some type of master controller prior to installation of the computer.



Additionally, a section consists of intersections which should always be coordinated with each other, but would not necessarily need to be coordinated with those of another section.

Although other types of signal systems were considered for Amarillo, the decision was made to install a computerized system. One of the reasons for this decision was the flexibility afforded by the computerized system. It would allow an unlimited number of different timing patterns to be utilized. A second reason was the availability of a large amount of surveillance data that are provided at the control center from the detectors in the street. A third reason for deciding on a computer system was its ability to interface with a wide variety of local intersection controllers which was considered to be important both with the initial installation as well as in future expansion of the system.

In comparison with other systems (Table 2) the Amarillo system appears more costly. Table 3 lists a breakdown of the principal cost items in the Amarillo system. The first item that will be observed is the extremely high cost of cable and conduit. This is discussed in Chapter II. Additionally, new poles, heads and local controllers were installed at many of the intersections, thereby raising the cost.

Prior to installation of the computerized signal system there were several different interconnected systems in operation. What became Section 1 in the computer system was controlled by the Automatic Signal Company's PR System. The PR is an analog system which can vary splits, offsets and cycle lengths based on varying traffic demands. Although it affords flexibility in providing different traffic signal patterns for

TABLE 3

COST OF PRINCIPAL ITEMS

| Item | Cost | | | | |
|------------------------------------|-------------|--|--|--|--|
| Cable and conduit | \$1,250,000 | | | | |
| Poles, heads and local controllers | \$ 450,000 | | | | |
| Computer and peripheral equipment | \$ 250,000 | | | | |

different conditions there were some problems encountered in trying to maintain good signal progression. Most of these problems were the result of the inability to obtain precise settings on the dials which controlled splits and offsets. The only way the desired split and offset could be accurately set was by using a stop watch. This created problems when it was necessary to change out a controller for maintenance. Since the dials did not afford precise timing the replacement controller may not have had the proper settings even though the technician would set it to the specified dial settings.

Section 2 was a Crouse-Hinds Trafflex System. This system worked quite well considering its age in excess of twenty years at the time of replacement. The system in Amarillo had the ability to vary cycle lengths but was limited to one split for each intersection. The cycle length was varied by increasing or decreasing the voltage on the secondary or "braking" coil which would allow the dial to turn at different speeds. The lower the secondary coil voltage, the faster the dial would turn which would therefore provide a short cycle length. The problem with this method of operation is the inability to precisely control the clearance intervals. For example, a five per cent clearance interval would give a yellow time of 2.25 seconds with a 45 second cycle and 4.5 seconds with a 90 second cycle.

Prior to placing it under computer control, Section 3 was also a PR system as described for Section 1. The system seemed to work somewhat better in this situation where the technician only had five signals to coordinate.

The north portion of Section 4 (3rd through 15th Street) was a trafflex system prior to computerization. The two intersections at I-40 and Washington along with Wolflin and Washington were controlled by a three dial electromechanical system. The two intersections of Washington at South 22nd and South 24th Avenues were independent semi-actuated controllers.

Sections 5 and 7 were three-dial electromechanical systems prior to being placed under computer control. These three-dial systems remained as back-ups after computerization.

CHAPTER II

DESCRIPTION OF COMPUTERIZED SIGNAL SYSTEM

Hardware

The majority of the local intersection controllers in the system are electromechanical fixed time controllers which, when under computer control, have the cam stacks ratcheted by the computer. This type of control requires the computer to stop the dial at the controller, via a pair of wires, and then issue advance pulses over a second pair of wires. A third pair of wires is required to return the A phase green status to the computer. There are 600 pairs of wire coming into the central computer room. There are several alternatives which could have been used to reduce the extremely large expense associated with this much conduit and cable. The possibility of leased telephone lines was rejected because of the large continuing expense of rental plus the lack of control over the reliability of telephone company wires. Multiplexing was rejected because it was thought to be inadequately proven from a dependability standpoint at the time the plans were prepared in 1973. Additionally, multiplexing would necessitate additional equipment for the traffic signal technicians to maintain.

Software

The software package the Amarillo system utilizes has four primary modes of operation. They are time of day, manual, static and dynamic. The time of day mode, of course, is the calling for a certain timing pattern to be implemented in a certain section at a certain time. Manual pattern selection is available whereby the operator calls a certain pattern up via the teletype. The static and dynamic modes are of a responsive nature and utilize traffic volume data from the system detectors to select a pattern. At the time the after data were collected all sections of the system were being operated in the time of day mode.

The software package also has the provision for critical intersection control (CIC) operation. This feature allows certain intersections to be designated as critical intersections and permits the splits to be varied by the computer based on demand on each phase. The intersection is still constrained to operate with the same cycle length as the rest of its section. The main disadvantage of this type of operation is that there must be at least one detector for each phase of operation.

Generally two sections of the system will be operating independently with no concern for progression between sections. There are numerous cases, however, where it is desirable to have progressive movement between two adjacent sections. This can be done by locking one section (a satellite section) to another (a key section) either manually or automatically. The automatic locking is implemented in the responsive modes when the cycle lengths of the key section and the satellite section come within a specified amount of each other (usually 5 to 10 seconds). This

happens as long as locking is permitted by the operator at that particular time.

The timing patterns which were implemented with the new system were obtained by using either the PASSAR II or SIGOP programs. Both of these are computer signal optimization programs. The SIGOP program was used in the downtown area (Sections 1 and 2) in that it was designed for use in a grid system. The PASSAR II program, being designed as an arterial optimization program was used on Sections 3 through 7.

Based on traffic volume counts it was found that, generally speaking, there were four different traffic demand characteristics during the day. These were found to be the morning (AM) peak, the noon peak, the afternoon (PM) peak and the off peak period. For the morning peak period a pattern was developed which favored inbound traffic. The noon peak required a pattern which did not favor any particular direction but provided a longer cycle length than necessary for the off peak periods to accommodate the heavier volume of traffic. The afternoon peak had the highest volume of traffic of the day and, therefore, required the longest cycle length. Also, it provided preferential movement in the outbound direction. The off peak pattern had the shortest cycle length and was designed to move traffic in all directions as much as possible. In all cases the streets with the higher volumes were favored in the development of traffic signal patterns.

CHAPTER III

EXPERIMENTAL DESIGN, DATA COLLECTION AND ANALYSIS METHODOLOGY

Experimental Design

The basic research question addresses itself to the ways and the extent to which a computer controlled traffic signal system improves traffic operations. This will be determined by investigating the effect the computerized signal system has on the following variables:

- 1. The number of stops.
- 2. The amount of vehicle delay.
- 3. The number of accidents.
- 4. The motor vehicle operating cost.

One possible way to study or investigate the effect of these parameters is to formulate the following questions:

Research Question 1 - Has the number of stops required by drivers been reduced by the installation of the computerized signal system?

Research Question 2 - Has there been a decrease in vehicle delay associated with the system?

Research Question 3 - Has there been a reduction in the number of accidents on the streets comprising the new signal system since its installation?

Research Question 4 - Does the reduction in Motor

Vehicle operational cost due to reduced stops and delay exceed the capital and operating cost of the system?

With regard to these research questions it is hypothesized

 The installation of the system will result in a reduction in the number of stops required.

that:

- 2. The new system will result in a reduction in vehicle delay.
- 3. There will be a reduction in accidents on the streets that are controlled by the signal system.
- 4. There will be a reduction in vehicle operating cost due to the installation of the signal system which will exceed the capital and operating cost of the system. It is proposed this be evaluated on an equivalent uniform annual cost basis with a ten year life of the signal system.

Each of these hypotheses may be stated statistically as follows:

| Null Hypothesis | Alternate Hypothesis |
|----------------------|----------------------|
| 1. $S_A = S_B$ | 1. $S_A < S_B$ |
| $D_A = D_B$ | 2. $D_A < D_B$ |
| $3. A_{A} = A_{B}$ | $A_A < A_B$ |
| 4. $C_B - C_A < C_S$ | 4. $C_B - C_A > C_S$ |

where, S_{A} = the number of stops required on the section of the system in question and for the time period being

- studied after installation of the computerized signal system.
- $\mathbf{S}_{\mathbf{B}}$ = the number of stops required on the section of the system in question and for the time period being studied before the installation of the computerized signal system.
- D_A = the number of seconds of delay incurred on the section of the system in question and for the time period being studied after installation of the computerized traffic signal system.
- ${
 m D}_{
 m B}$ = the number of seconds of delay incurred on the section of the system in question and for the time period being studied before installation of the computerized traffic signal system.
- $A_{\underline{A}}$ = average annual number of accidents in the signal system in the after period.
- $A_{\overline{B}}$ = average annual number of accidents in the signal system in the before period.
- ${\tt C}_{\tt B}$ = the vehicle operating cost of driving on the system prior to installation of the computerized signal system for all vehicles during all time periods for one year.
- ${f C}_{f A}$ = the same vehicle operating cost as above after installation of the computerized traffic signal system.

C = the equivalent uniform annual cost of the capital
 and operating expense of the system assuming a ten
 year life.

The data for this study were based on travel time runs on each section of roadway that was put under computer control. These runs were made utilizing the "average car" method. They consist of runs prior to as well as after installation of the computerized traffic signal system. Each street had six runs in the before period and six runs in the after period, as recommended in the Traffic Control System Handbook (3, p. 578).

There were runs for each of the following time periods: morning peak, noon peak, evening peak and off peak. The Traffic Control
System Handbook suggests six runs in the peak period and six runs in the off peak period. In this study, however, it is believed there should be separate runs in each of the three previously mentioned peaks as well as the off peak primarily because there will be separate timing patterns for each peak period when under computer control. The only way that this can satisfactorily be taken into account is by making a separate study during each period.

The travel time runs were conducted using the "average car" technique. In this procedure the "vehicle travels according to the driver's judgement of the average speed of the traffic stream" (10, p. 100). "Tests of this method have shown excellent correlation with actual average travel time" (11, p. 427).

Using the travel time data the number of stops and amount of stopped time delay during each of the time periods mentioned were

computed. These values were determined for both the period prior to as well as after placing the signals under computer control and were statistically compared. The motorists' operating cost (moc) was then computed as follows:

$$moc = (s)(c_s)(v) + (d)(c_d)(v)$$

where, s = number of stops per vehicle

c = cost per stop

v = annual volume

d = stopped time delay per vehicle

c_d = cost per vehicle second of delay

Appropriate cost figures for stops and delay and the total cost to the motorists before placing the system under computer control can be determined.

This analysis was repeated to obtain the motorists' operating cost after placing the system under computer control. The difference between the operating cost to the motorists in the before and after period can then be computed and compared with the equivalent uniform annual cost of the capital and operating expenses of the computerized signal system.

In a study such as this where the data collection for the two situations is done with a considerable time lapse it is not expected that traffic volumes would remain constant. The changes in traffic volumes should be small enough to assume the same volumes for both the before and after period. The alternative to this would be to attempt to measure the traffic volumes during each time period (AM Peak, Noon Peak, PM Peak and Off Peak) for both the before and after periods. This would

introduce more error into the analysis than using the same volume for both the before and after period because the traffic volumes that were used were typical daily volumes on each particular street. They were not true average daily traffic (ADT) values in that the only way true ADT values could be obtained would be to count the total yearly volume on the street and divide by 365 days per year. Since this is not practical, weekday traffic volume was used. If another typical weekday volume was used for the after period, the daily and monthly variations that would occur might introduce more error than would be avoided by using new counts in the after period. It is reasonable to assume that there is a slight increase in volumes annually. For this reason any reductions observed in stops, delay, accidents or motorists' operating cost would be somewhat on the conservative side.

Research Question 1

The travel time data consist of six runs along each street during each of the time periods previously described. The average number of stops for the six runs during each time period for each street was computed. Repeating this process for all time periods gives the total number of stops in an average day on that particular street. In a similar manner the total number of stops was calculated for an average day after the new signal system was operational. The first null hypothesis, $S_A = S_B$ may now be statistically evaluated with the alternate hypothesis being $S_A < S_B$. This can be done using the student's tdistribution significance test (12, p. 136). This will be a one tailed test with a 0.05 significance level which will be performed separately

for each time period of each street and then for a total average day for each street.

A comparison of the grand total number of stops for the entire system in the before and after periods can be made by utilizing the chi square test (12, p. 205). In this test the number of stops in the before period would be entered as the expected values while those in the after period for each street would make up the observed values. This chi square evaluation would be made at the 0.05 significance level.

Additionally a t-test may be used to evaluate the number of stops in the after period with respect to the number of stops in the before period for the entire system.

Research Question 2

This test will be similar to the one in Research Question 1 except that the quantity being measured will be the number of seconds of stopped-time delay. The number of seconds stopped will be measured for each of the six runs on each street. An average number of seconds of stopped-time delay will then be computed for each street during each time period by dividing the total number of seconds of stopped-time delay for the six runs by six. This average number of vehicle-seconds of delay per vehicle during each time period when multiplied by the number of vehicles on the street during that time period will give the total amount of delay on that street during that time period.

The null hypothesis of $D_A = D_B$ may now be evaluated with the alternate hypothesis of $D_A < D_B$ where $D_A =$ the number of vehicle seconds of stopped time delay in the six runs in the after period and $D_R =$ the

number of vehicle-seconds of stopped-time delay in the six runs in the before period. This evaluation can be made with a one-tailed t-test at a 0.05 significance level for the entire system.

Research Question 3

In this test the number of accidents on the streets comprising the signal system in the before versus the after period will be compared. The before period is the three year period from January 1, 1972 through December 31, 1974. The after period is January 1, 1976 through December 31, 1978. The calendar year 1975 is excluded from comparison because the installation of the signal system was underway during most of that year. The significance test which is appropriate when there is a three year before and a three year after time period is the Poisson test (13, p. 47). When it is necessary to analyze data consisting of large numbers the Poisson test, as performed by Gerlough (14, p. 50) becomes quite cumbersome and may be approximated by the formula:

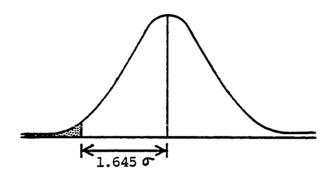
$$(B - A) > 1.654 \sqrt{M}$$

where B = number of accidents in the before period

A = number of accidents in the after period

M = mean number of accidents

This formula is based on the fact that the mean is equal to the variance for the Poisson distribution (15, p. 107). The standard deviation is therefore the square root of the mean (\sqrt{M}) . In order to have one-tailed significance at the 0.05 significance level the difference in the accidents in the two periods must be greater than 1.645 times the standard deviation (i.e. $1.645 \sqrt{M}$). This is graphically depicted in Figure 2.



B-A $> 1.645\sqrt{M}$ for significance at 0.05 level

Fig. 2 - Significance test for reduction in accidents

Research Question 4

The answer to this question is the basic goal of this research project. It draws from the answers to Research Questions 1, 2 and 3. It will be measured in terms of an equivalent uniform annual cost of motorists operating on the streets having computerized control with the equivalent uniform annual cost of the previous system. Any reduction of equivalent uniform annual motorists' operating cost will be compared with the difference in equivalent uniform annual capital and operating cost of the new versus the old signal systems. This analysis will utilize the vehicle operating cost data of Winfrey (4) and the more up to date (1975) cost data published by AASHTO (17).

CHAPTER IV

ANALYSIS OF RESEARCH QUESTIONS

Research Question 1

The first research question which compares the number of stops in the before period with the after period on each street was conducted using the Student's t-test. Table 4 shows the number of stops during the before and after periods on a typical street (Adams) in the north-bound direction during the AM Peak. Table 5 shows the same information summarized by section.

This t-test is performed with paired variates, one in the before period and one in the after. The t-distribution in this instance is defined (12, p. 146) by:

$$t = \frac{\overline{D} - m_d}{S_{\overline{d}}}$$

where, $\overline{\mathbf{D}}$ = mean of the differences between each before and after pair in the sample

 m_{d} = difference in the population mean

 $S_{\overline{d}}$ = best estimate of standard deviation of mean of population differences

or

TABLE 4

ADAMS STREET-NORTHBOUND AM PEAK

| Run Number | No. Stops Before | No. Stops After | Difference (D) Before-After |
|---------------|---------------------|--------------------|--------------------------------|
| 1 | 2 | 0 | 2 |
| 2 | 1 | 0 | 1 |
| 3 | 1 | 0 | 1 |
| 4 | 1 | 1 | o |
| 5 | 1 | 0 | 1 |
| 6 | 1 | 0 | $\frac{1}{\Sigma D = 6}$ |
| n = 6 | | | $\bar{D} = 1$ |

TABLE 5

BEFORE-AFTER COMPARISON OF STOPS AND DELAY IN SIX
TRAVEL TIME RUNS DURING EACH TIME PERIOD

| | Stops (Number) Delay (Vehicle-Seconds) | | | | | | | | | | | | | | |
|---------|--|-------|--------|-----------|-------|---------|--------|----------|--------|--------|-------|--------|--------|-------|--------|
| Section | AM Peak | | | Noon Peak | | PM Peak | | Off Peak | | | Total | | | | |
| S | Before | After | Change | Before | After | Change | Before | After | Change | Before | After | Change | Before | After | Change |
| 1 and 2 | 375* | 318 | -57 | 496 | 250 | -246 | 382 | 320 | -62 | 378 | , 363 | -15 | 1631 | 1251 | -380 |
| | 5961 | 6281 | +320 | 5436 | 3870 | -1566 | 6676 | 7115 | +439 | 7876 | 3953 | -3923 | 25949 | 21219 | -4730 |
| 3 | 7 | 0 | -7 | 3 | 1 | -2 | 7 | 13 | +6 | 0 | 0 | 0 | 17 | 14 | -3 |
| | 17 | 0 | -17 | 8 | 2 | -6 | 81 | 89 | +8 | 0 | 0 | 0 | 106 | 91 | -15 |
| 4 | 17 | 9 | -8 | 26 | 20 | -6 | 31 | 38 | +7 | 12 | 12 | 0 | 86 | 79 | -7 |
| | 113 | 73 | -40 | 239 | 335 | +96 | 560 | 776 | +216 | 181 | 219 | +38 | 1093 | 1403 | +310 |
| 5 | 24 | 2 | -22 | 34 | 14 | -20 | 31 | 19 | -12 | 25 | 5 | -20 | 114 | 40 | -74 |
| | 430 | 9 | -421 | 818 | 411 | -407 | 1071 | 159 | -912 | 355 | 32 | -323 | 2674 | 611 | -2063 |
| 7 | 9 | 0 | -9 | | - | | 7 | 9 | +2 | 6 | 7 | +1. | 22 | 16 | -6 |
| | 152 | 0 | -152 | - | _ | - | 186 | 61 | -125 | 177 | 52 | -125 | 515 | 113 | -402 |

^{*}The numerator represents stops (number) and the denominator represents delay (vehicle-seconds).

$$S_{\overline{d}} = \frac{S_{\overline{d}}}{\sqrt{n}}; \quad S_{\overline{d}} = \sqrt{\frac{\sum (D - \overline{D})^2}{n - 1}}$$

where, S_d = best estimate of standard deviation of population differences

n = sample size

$$S_{\bar{d}} = \sqrt{\frac{(1)^2 + 0 + 0 + (-1)^2 + 0 + 0}{5}} = \sqrt{.4}$$

$$S_{\bar{d}} = \frac{S_{\bar{d}}}{\sqrt{n}} = \frac{\sqrt{.4}}{\sqrt{6}} = \sqrt{.0667} = .258$$

$$t = \frac{\overline{D} - 0}{S_{\bar{d}}} = \frac{1}{.258} = 3.88$$

Using five degrees of freedom (N - 1) the table value for t $_{.05}$ = 2.015. Since the calculated t-value of 3.88 is greater than 2.015, it falls in the rejection area as shown in Figure 3. For this reason the null hypothesis of $S_A = S_B$ is rejected and the alternate hypothesis of $S_A < S_B$ is accepted. In a similar manner the null hypothesis of $S_A = S_B$ was evaluated for each street in each direction during each time period. These calculations are shown in Appendix C.

A t-test was also used to evaluate the total number of stops on all streets during all time periods. This was performed by computing the difference between the total number of stops in the six runs in the before period with the number of stops in the six runs in the after period for each time period of each street in each direction. For example, in the northbound direction on Adams during the AM peak there were seven stops recorded in the six runs in the before period and one stop in the six runs in the after period. The difference in these two values is 6. This procedure is repeated for all streets in all time periods for the

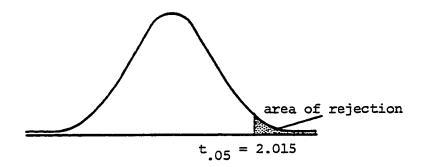


Fig. 3 - Significance test for reduction in stops

entire system. The mean of all the differences is then computed. The t-test can then be applied in the same manner as for the individual street and time periods as described previously. The calculation of this t-test is shown in Appendix D.

The total number of stops before and after during each time period on each street was computed by multiplying the volume during each period by the number of stops per vehicle during each period. These values were summed for each section to give the total number of stops per day on each section in both the before and after period. The number of stops per day in each section was then summed to give the total number of stops per day on the entire system both for the period prior to the installation of the computerized traffic signal system as well as after its installation. This permits the comparison of the stops in the system considering the volume of traffic on the various streets rather than simply comparing the number of stops in a fixed number of runs down a particular street. The total number of stops in the after period was subtracted from the number of stops in the before period to obtain the reduction in the total number of stops that could be expected on an average day of operation of the computerized traffic signal system. reduction was then expressed in the form of a percentage reduction and the comparison is shown in Table 6.

A chi square analysis is also presented comparing the number of stops in the before versus the after period of all streets in all time periods in total. As in the t-test for the entire system the purpose of this analysis is to compare statistically the number of stops for the entire system in the before period with the after period. This analysis is shown in Appendix E.

TABLE 6
STOP AND DELAY COMPARISON BY SECTION

| <u></u> | | Stop Day | _ | | I | Delay (| (eh-Hr Day | |
|---------|---------|-------------|----------------|-------|---------|---------|---------------|----------|
| Section | Dofo | A.5 | Cha | nge | Before | 15000 | Cha | ange |
| | Before | After | Number PerCent | | perore | After | Number | Per Cent |
| 1 and 2 | 290,687 | 235,420 | -55,267 | -19.0 | 1,335.9 | 892.4 | -443.5 | -33.2 |
| 3 | 2,232 | 2,417 | +185 | +8.3 | 4.1 | 4.5 | +0.4 | +0.9 |
| 4 | 16,890 | 15,166 | -1,724 | -10.2 | 64.6 | 74.5 | +9.9 | +15.3 |
| 5 | 35,901 | 10,648 | -25,253 | -70.3 | 200.1 | 31.3 | -168.8 | +84.4 |
| 7 | 8,374 | 8,327 | -47 | -0.6 | 60.1 | 16.4 | -43.7 | -72.7 |
| Total | 354,084 | 271,978 | 82,106 | -23.2 | 1,664.8 | 1,019.1 | -645.7 | -38.8 |

Research Question 2

In a manner similar to that used in Research Question 1 the vehicle-seconds of delay in the before and after periods was compared using the t-test. This analysis is performed in Appendix G with a summary presented in Table 5. The total number of vehicle-hours of delay in each time period on each street was then obtained in both the before and after periods by multiplying the delay per vehicle by the volume during the time period. Again, this value was summed to obtain the number of vehicle-hours of delay on each section during each time period and for the entire day for both the before and after periods. It was then, summed for all sections to give the total system delay per day in both the before and after periods. The percentage reduction in delay was then computed for the entire day.

Research Question 3

Table 7 shows the number of accidents by year on each section of the city where the computerized traffic signal system was installed. Since the signal system was installed in 1975, that particular year was excluded from the comparison of accidents. The average annual number of accidents on the entire system in the before period (1972-1974) was 1216. The average annual number of accidents in the after period (1976-1978) is 1139. This would be a reduction of an average of 77 accidents per year in the after period which on the basis of an average annual number of accidents of 1216 yields a 6.3 per cent reduction. This is a significant reduction in accidents at the 0.05 significance level using the

TABLE 7
YEARLY ACCIDENTS BY SECTION

| Year | | | Section | on. | | | |
|--------------------------|-------|-------|---------|-------|-------------|------|-------|
| | 1 & 2 | 3 | 4 | 5 | 6 | 7 | Total |
| 1972 | 747 | 52 | 151 | 103 | 15 | 100 | |
| 1973 | 784 | 68 | 177 | 98 | 21 | 104 | |
| 1974 | 737 | 78 | 163 | 134 | 27 | 89 | |
| Σ 72,73,74 | 2268 | 198 | 491 | 335 | 63 | 293 | 3648 |
| 1976 | 704 | 95 | 163 | 139 | 29 | 123 | |
| 1977 | 643 | 99 | 162 | 143 | 38 | 108 | |
| 1978 | 530 | 85 | 130 | 113 | 31 | 83 | |
| Σ 76,77,78 Percent | 1877 | 279 | 455 | 395 | 98 | 314 | 3418 |
| Change | -17.2 | +40.9 | -7.3 | +17.9 | +55.6 | +7.2 | -6.3 |

Poisson distribution significance test for accidents. A further summary of accidents in the two periods is shown in Table 8. As can be observed, the downtown area (sections 1 and 2) is the only one to realize a significant reduction in accidents and in fact realized such a decrease in accident it was largely responsible for the significant accident reduction for the entire system.

There are two items that must be considered in this accident analysis. The first is that although certain sections show an increase in the number of accidents, they are areas that have had a general increase in traffic volumes. It is not unreasonable to assume these increases in accidents to be generally proportional to the increased traffic volumes therefore resulting in similar accident rates for the two periods. The second is that although the Poisson distribution test reveals a significant accident reduction in the after period, the conclusion may not be drawn that the reduction is due to the new signal system.

Another item that could partially account for the accident reduction is the selective traffic enforcement program (STEP) that was initiated at generally the same time period as the new signal system. In this particular program the State of Texas subsidized the City for the salary of off-duty policemen to increase enforcement of traffic laws at particular locations that have an accident problem.

It is interesting to examine the percentage of accidents that occur on the streets controlled by the signal system compared to the total number of accidents in the city. These data are shown in Table 9 and point out that system accidents varied from a high 19.9 percent of total accidents in 1974 to a low of 15.2 percent of total accidents in 1978. In the before period (1972-1974) accidents occuring on the streets which

TABLE 8
SIGNIFICANCE TESTS OF ACCIDENT REDUCTION

| | | | | Sect | ion | | | |
|---|-------|-----|-----|------|-----|-----|--------|------------|
| | 1 & 2 | 3 | 4 | 5 | 6 | 7 | Tota | a l |
| | | | | | | | System | City |
| Average Before (1972-1974) | 756 | 66 | 164 | 112 | 21 | 98 | 1216 | 6597 |
| Average After (1976-1978) | 626 | 93 | 152 | 132 | 33 | 105 | 1139 | 6879 |
| Difference | -130 | +27 | -12 | +20 | +12 | +7 | -77 | +282 |
| Significant Reduction at 0.05 Level | Yes | | No | | | | - Yes | |
| Significant Increase at 0.05 Level | | Yes | | Yes | Yes | No | | Yes |

TABLE 9
ACCIDENT SUMMARY

| ** | | s | ectio | n. | | | Tota | 1 | Per Cent Acci- |
|------|-------|----|-------|-----|----|-----|---------|------|-------------------------------|
| Year | 1 & 2 | 3 | 4 | 5 | 6 | 7 | Systems | City | dents on System to Total City |
| 1972 | 747 | 52 | 151 | 103 | 15 | 100 | 1168 | 6244 | 18.7 |
| 1973 | 784 | 68 | 177 | 98 | 21 | 104 | 1252 | 6693 | 18.7 |
| 1974 | 737 | 78 | 163 | 134 | 27 | 89 | 1228 | 6855 | 19.9 |
| 1975 | 745 | 91 | 171 | 147 | 15 | 109 | 1278 | 6877 | 18.6 |
| 1976 | 704 | 95 | 163 | 139 | 29 | 123 | 1253 | 7044 | 17.9 |
| 1977 | 643 | 99 | 162 | 143 | 38 | 108 | 1193 | 7211 | 16.5 |
| 1978 | 530 | 85 | 130 | 113 | 31 | 83 | 972 | 6382 | 15.2 |

were to be controlled by the signal system comprised 18.4 percent of the total accidents in the city. In the after period (1976-1978) this figure had dropped to 16.6 percent. This reduction in the percent of total city accidents that occur in the signal system tends to support the hypothesis that the reduction in accidents was due to the signal system rather than the STEP program since it would be expected that the STEP program would reduce accidents more equally throughout the city. It is possible, however, that a disproportionately large portion of the emphasis of the STEP program was on the same streets that were placed under computer control therefore partially accounting for the reduction on those streets.

Research Question 4 - Basic Considerations

In answer to this research question, the annual motorists' operating cost was computed for the system for both the period before as well as after installation of the computerized traffic signal system. This was done by computing the total cost of the stops and vehicle delay to the motorists. The cost of the vehicle delay is computed by summing the excess idling cost brought about by the stopped time delay with the time value of the delay to the motorists. The actual cost of driving through the system at a constant speed was not included since it is the same for both periods and eventually cancels itself out of the analysis.

In order to obtain the cost of stops and delay it was assumed that there were 10 percent trucks and a cost value for trucks was obtained by averaging the cost values of single unit and 40 kip trucks. This figure is not inconsistent with the values obtained in manual

counts on the streets in the system. The only alternative to this assumption would be to collect the actual percentage of trucks on each street on the system. This would be a very difficult procedure and would not substantially improve the accuracy of the results since very minor changes would be expected in the percentage of trucks in the two periods. It was also assumed that the stops were for 25 miles per hour with the vehicle returning to that speed after the stop.

Research Question 4 - Quantification

The calculation of the motorists' operating costs on the system in the two time periods is shown in Appendix I. The annual cost in the before period was found to be \$2,254,283 and in the after period was calculated at \$1,624,849. The difference in these two values (\$629,434) is therefore the calculated annual cost savings to the motorists with the new system.

The cost values (\$6.96 per 1000 stops for passenger cars, etc.) are taken from Winfrey (4, p. 688, 700, 723). The \$1.00 per vehicle hour is the minimum value of the range of \$1.00 - \$4.00 per vehicle-hour given by Winfrey (4, p. 269).

The total cost of the project was \$1,958,000 (18). Assuming a ten year life of the installation the equivalent uniform annual cost of the required capital expenditure (assuming 8 percent interest) is \$291,800.

A benefit-cost analysis may be performed by comparing the benefits derived in the form of reduced motorists' operating costs per year to the annual cost of the system. In order to do this the increased maintenance and operating cost of the computerized signal system must be included. The increased maintenance cost is due to the highly technical and specialized nature of a digital computer and its peripheral equipment. Maintenance of this type of equipment is beyond the scope of the capabilities of a typical city's traffic signal shop. Additionally in order to fully utilize such a system extra effort in developing signal timing patterns is required by the city's staff. The total increased cost of maintenance and operating support is estimated to be \$40,000 per year. Using these figures the benefit—cost ratio of the system in question may be computed as follows:

$$B - C = \frac{\text{Reduced Annual Motorists' Operating Costs}}{\text{EUAC for Installation + Increased Maintenance and Operating Cost}}$$

$$B - C = \frac{\$629,434}{\$291,800 + \$40,000} = \frac{\$629,434}{\$331,800}$$

$$B - C = 1.90$$

Although the assumption of a ten year life is valid for the digital computer itself and its peripheral equipment, it is not valid for the rest of the system equipment. The conduit and cable installation which comprised a large portion of the project cost (\$1,250,000) would have a useful life of approximately 30 years. The traffic signal poles, heads and local controllers which would have a useful life of approximately 20 years represented an investment of approximately \$450,000. The remaining \$258,000 of the total project cost represents the cost of the computer and peripheral equipment. As previously stated, the estimate of a ten year life is reasonable for that portion of the project. Using these values for useful life, the equivalent uniform

annual cost for the project is \$194,124. These calculations are shown in Appendix I.

Using this value for the equivalent uniform annual cost of the installation and the same values for reduced motorists' operating costs and increased maintenance and operating costs the benefit-cost ratio can be computed.

$$B - C = \frac{\text{Reduced Annual Motorists' Operating Costs}}{\text{EUAC for Installation + Increased Maintenance and Operating Cost}}$$

$$B - C = \frac{\$629,434}{\$194,124 + \$40,000} = \frac{\$629,434}{\$234,124}$$

$$B - C = 2.69$$

One shortcoming of the preceding analysis is that it is based on cost figures presented by Winfrey (4) in his book published in 1969. Since the system being evaluated was installed in 1975 the vehicle operating cost data are well out of date. A 1978 publication by AASHTO (17) provides vehicle operating cost data for a 1975 base year. Repeating the preceding analysis using the AASHTO cost figure (17, p. 132, 133, 134, 171, 17) yields motorists' operating costs in the before and after periods respectively of \$2,452,362 and \$1,823,823.

In this analysis the figure of \$0.21 per traveler-hour is reccommended by AASHTO for time savings of zero to five minutes on average trips. Additionally on an average of trip purposes a value of 1.56 adults per vehicle is recommended (17, p. 17).

Therefore, it is observed that although different values are used in the AASHTO publication from the Winfrey book, the end result is almost identical (\$628,539 verses \$629,434). A benefit-cost analysis

will not be performed on the figures obtained using the AASHTO values since the results would be almost identical to those previously done.

Another method of analyzing the economics of the improvement is the internal rate of return analysis (19, p. 267). In this method the benefits are related to the costs not in the form of a ratio, but rather in the form of an annual percentage return on the investment over the life of the improvement. Again using a ten year life of the system the annual rate of return as computed in Appendix I is 27.4%.

Another important consideration in the analysis of a project such as this is the effect the new signal system has on fuel consumption and air pollution. Appendix J contains the calculations that reveal a reduction in gasoline consumption of approximately 1200 gallons per year with the installation of the new signal system. This is based on the figures of 0.58 gallons consumed per vehicle-hour of idling and 0.01 gallons consumed per vehicle-stop. Both of these figures are presented by Claffey (8).

Appendix K is the calculation of the reduction in air polution that might be expected from the more efficient vehicle operation associates with the new signal system. It reveals an approximate reduction in hydrocarbons (HC) emitted of 6.4 pounds per year and a reduction in carbon monoxide (CO) of approximately 1588 pounds per year. These figures were calculated in the manner recommended by Curry and Anderson (20, p. 38).

CHAPTER V

RESULTS

In consideration of the four basic Research Questions that were posed in Chapter II it is appropriate that an examination of the results of the analysis of Chapter IV be made.

Research Question 1

It is observed by examining the results of the t-test in Appendix C some of the streets during some of the time periods realized a significant reduction in the number of stops while others did not and in fact realized an apparent increase in the number of stops. The increase in the number of stops on some streets during some time periods is not surprising and in fact may be necessary to some extent in order to improve the operation of the streets and/or directions carrying the higher volumes. The timing patterns which were placed in the computer (those in the after period) were totally new patterns that were obtained using computer programs that optimize traffic signal timing patterns. When installing a new signal timing pattern in an area that previously had a progressive system it is expected that certain directions and/or streets would have an increase in the number of stops per travel time rum in order that there could be a reduction in the number of stops on

those streets and/or directions with higher volumes. This, of course, would result in a reduction in the total number of stops on the system.

The answer to Research Question 1 lies in the analysis of the total number of stops in the entire system considering all time periods and directions. This analysis reveals a reduction in the number of stops in the after period that is significant at the 0.001 level. The implication of this analysis is that it can be stated that the number of stops in the after period (under computer control) is less than in the before period with a one in one thousand chance of committing a type I error (12, p. 126). As shown in Figure 4, the calculated t-value of 5.47 is well into the rejection region which leads to rejection of the null hypothesis. In the interest of statistical accuracy it should be stated that the t.001 value of 3.373 would actually give a 0.0005 significance level since the analysis is a one-tailed test and the 0.001 portion of the area under the curve is the area under both tails of the curve.

Therefore, the response to research question number one is that the number of stops required by drivers has been reduced with the installation of the computer controlled traffic signal system.

Research Question 2

As in the analysis of Research Question 1 the most powerful test for this question is the t-test. As in the analysis for the number of stops a t-test could be performed on the individual streets however there is such a wide range of values the results would be of very little meaning. A t-test analysis on vehicle-seconds of

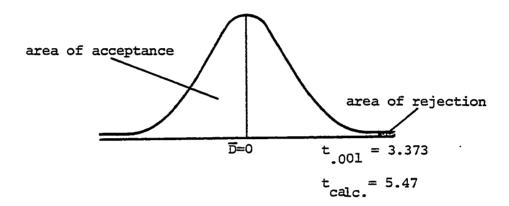


Fig. 4 - t-test of reduction of stops in the entire system

delay for the entire system is meaningful and was performed (Appendix G). Examining the null hypothesis that the delay in the after period is equal to the delay in the before period ($D_A = D_B$) against the alternate hypothesis that the delay in the after period is less than the delay in the before period ($D_A < D_B$) the t value is computed to be 2.87. This infers that the delay in the after period is significantly less than the delay in the before period at the 0.01 significance level (Figure 5).

Research Question 3

As was pointed out in Chapter IV there was a significant reduction in the number of accidents in the after period (1976-1978) when compared to the before period (1972-1974). It was also pointed out that there were other factors present which could have at least partially accounted for the reduction in accidents (e.g. selective traffic enforcement program). That the percentage of accidents on the system compared to the total number of accidents in the city decreased from 18.4 percent before to 16.6 percent after supports the conclusion that there was in fact an accident reduction due to the installation of the computerized traffic signal system and associated local intersection hardware.

The reduction in accidents could be the result of several factors. First, better progression on a street should result in fewer rearend collisions. This is due to the fact that if the number of stops is reduced the likelihood of a rear-end collision is also reduced. Second, the timing with the new system is more precise. This is of particular

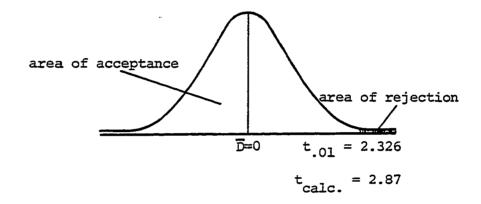


Fig. 5 - t-test analysis on $H_o: D_A = D_B$ with $H_A: D_A < D_B$

importance with the clearance intervals which is too short could lead to right angle and rear-end collisions. The possibility of short clearance intervals particularly with the Trafflex system was discussed in Chapter I.

A third, and a very important possibility for the reduction of accidents with the new system, is the installation of new mast arms and signal heads where they were necessary. This is particularly important where the old heads might have been difficult for the motorists to see. Certainly a motorist must be able to see a traffic control device before being expected to observe it. Most of the signal poles and heads in the downtown area (Sections 1 and 2) were replaced with more visible mast arm supported signal heads. That this portion of the system realized the largest decrease in accidents supports this as being the primary reason for the reduction in accidents.

Research Question 4

As shown in Chapter III, the benefit-cost ratio for the project was computed to be 1.9 based on a ten year life of the system. Using the following useful life for the various components of the system the benefit-cost ratio was calculated to be 2.7.

| <u>Item</u> | Useful Life |
|---------------------------------|-------------|
| Conduit and Cable | 30 years |
| Poles, Heads, Controllers | 20 years |
| Computer & Peripheral Equipment | 10 years |

Using a rate of return analysis and a 10 year system life the investment in the digital computerized traffic signal system yielded a 27.4 per cent return in the form of reduced motorists' operating costs.

It is interesting to compare the analysis using cost data from Winfrey (4) which is a 1969 reference with that using cost data from AASHTO (17) which was published in 1978. Table $10\,\mathrm{summarizes}$ this comparison. Comparison of Winfrey and AASHTO cost figures derived from computing for an average of trip purpose (1.56 $\frac{\mathrm{Adults}}{\mathrm{Vehicle}}$) and a time savings of 0-5 minutes on an average trip purposes (\$0.21 per traveler hour).

Summary of Results

Table 11 is a summary of each of the four research questions posed in this study. It can be observed that stops, delay, and accidents were significantly reduced. The system resulted in a benefit-cost ratio of 2.7 and yielded a 27.4 per cent rate of return.

The operating costs are higher in the 1978 AASHTO (17) publication than the 1969 Winfrey book (4) for passenger cars as would be expected with increases in fuel, oil, maintenance and capital cost of vehicles. In the total cost analysis however this increase is offset by the much lower excess passenger travel time value recommended by AASHTO. Although Winfrey does not specify an exact value for passenger car travel time he does give a range of \$1.00 to \$4.00 per car-hour (4, p. 269). The AASHTO publication has values more similar to this for higher time savings. For example, if a higher time savings (over 15 minutes) is to be realized on an average of trip purposes, the AASHTO value would be

TABLE 10

COMPARISON OF MOTORISTS OPERATING COSTS

| | Winfrey | AASHTO |
|--|---------------|--------|
| Cost per 1000 Stops - 4 kip Passenger Car | 6.96 | 11.25 |
| Cost per 1000 Stops - 12 Kip Truck | 17.65 | 26.50 |
| Cost per 1000 Stops - 50 kip (Winfrey) & 54 kip (AASHTO) Truck | 74.75 | 91.04 |
| Excess Idling Cost-Dollars/1000 Hours - 4 kip | 114.86 | 312.64 |
| Excess Idling Cost-Dollars/1000 Hours - 12 kip | 200.03 | 277.44 |
| Excess Idling Cost-Dollars/1000 Hours - 50 kip (54 kip) | 196.28 | 193.07 |
| Excess Travel Time Cost-Dollars/Veh-Hr. | \$1.00-\$4.00 | \$0.33 |

TABLE 11

IMPACT OF AMARILLO COMPUTERIZED SIGNAL SYSTEM

| Factor | Change | Significance |
|-------------------|------------|--------------|
| Stops | -23% | Yes |
| Delay | -39% | Yes |
| Accidents | - 6% | Yes |
| Annual User costs | -\$629,434 | N.A. |

(\$3.90 per Traveler-Hour) (1.56 $\frac{\text{Adult}}{\text{Vehicle}}$) = \$6.08 per vehicle-hour. (17, p. 17). Even with these differences the final result of the two methods is very similar and yields a similar payoff of the capital investment.

CHAPTER VI

CONCLUSIONS AND RECOMMENDATIONS

This study evaluated the impact on traffic operations of a computerized traffic signal system in Amarillo, Texas (population 150,000). The system consists of 133 intersections in seven sections controlled by a digital computer. On the basis of data collected and evaluated over an extended period of time the following conclusions were drawn:

- 1. There was an improvement in the traffic operation of the streets that were controlled by the computerized traffic signal system. The total number of stops which were made by all motorists driving on the streets placed under computer control was reduced by 23 percent. The number of vehicle-seconds of delay while stopped at the traffic signal was reduced by 39 percent. There was also a 6 percent reduction in the number of accidents in the three year period after installation of the computerized system as compared to the three year before period.
- 2. The improvement in stops and delay results in a reduction in annual motorists operating cost of approximately \$629.434.

- 3. The reduction in motorists' operating costs whem compared to the equivalent uniform annual cost of the system resulted in a benefit-cost ratio of 2.7 and a rate of return of 27.4 percent.
- 4. The capital cost of the computerized traffic signal system was larger than for other traffic signal control strategies.
- 5. The maintenance of the computer and peripheral equipment is very complicated and cannot normally be handled by the cities' maintenance staff. This normally means a contract with a computer maintenance firm at a cost of \$20,000 to \$40,000 per year.
- 6. The successful utilization of such a system normally requires one full-time operator.
- 7. The tremendous capabilities provided by a digital computerized traffic signal system must be largely utilized in order
 to justify the system. This means constantly improving the
 traffic flow by trying new patterns and using the information the computer obtains from detectors (e.g., stops and
 delay) to control a new pattern to an old one.
- 8. The improvements from the installation of the system can result only when the city understands and accepts the responsibility of providing funds for initial cost, maintenance and operating cost as a total package. If this is not realized, the installation will be of minimal benefit in which case other types of control systems such as fixed time multi-dial systems operated in a time of day mode or

arterial street systems with background coordination units should be explored. It should be pointed out, though, that the costs savings to the motorists are based on vehicle operating costs which are approximately ten years out of date. This leads to a conservative estimate of the benefit-cost ratio. With the rapid increase in gasoline and other vehicle expenses as well as the relative decline in computer equipment, systems which might not have resulted in a favorable benefit-cost ratio a few years ago might now be more cost effective. Consequently, such systems are becoming more feasible for the smaller cities than they have been in the past.

9. The companies that provide these systems should strive to make them simpler for the operator to input data and make changes to encourage a fuller utilization of the capabilities.

The above conclusions lead to the formulation of recommendations for further study which should consider the cost and effectiveness of other types of systems. For example, systems with other methods of communication (multiplexing, leased telephone lines, laser beam transmission, etc), which have a significantly lower initial cost, could be evaluated. Similarly, it would be worthwhile to evaluate computer systems with the processors at remote field locations controlling the intersections and transmitting the survelliance data back to the central processor.

BIBLIOGRAPHY

- 1. Pignataro, Louis J. <u>Traffic Engineering Theory and Practice</u>. Prentice Hall, Inc., Englewood Cliffs, New Jersey, 1973.
- 2. Stockfish, Charles Ray. <u>Selecting Digital Computer Signal System.</u>
 U.S. Department of Transportation, Federal Highway Administration,
 1972.
- 3. Traffic Control Systems Handbook. U.S. Department of Transportation, Federal Highway Administration, Washington, D.C., 1976.
- 4. Winfrey, Robley. Economics Analysis for Highways. International Textbook Company, Scranton, Pennsylvania, 1969.
- Dudek, Conrad L. and McCasland, W. Richard, "Cost-Effectiveness of Freeway Merging Control." <u>Highway Research Board Record</u> 363, 1971, pp. 43-59.
- 6. Evans, Leonard, Herman, Robert and Lam, Tenny. "Multivariate Analysis of Traffic Factors Related to Fuel Consumption in Urban Driving," Transportation Science, Vol. 10, No. 2, May, 1976, 205-215.
- 7. Norman, Mark R. and Bulman, David H. "Improvement of Traffic Flow to Reduce Energy Use." <u>Compendium of Technical Papers</u>. Institute of Transportation Engineers 46th Annual Meeting, Baltimore, Md., August, 15-19, 1976.
- Claffey, Paul J. "Running Costs of Motor Vehicles as Affected by Road Design and Traffic." NCHRP Report 111, Highway Research Board, 1971.
- 9. Lee, Jim C. "Computerized Traffic Signal System for Amarillo, Texas." ITE Technical Notes, Volume I, No. 4, July, 1976.
- 10. Box, Paul C. and Oppenlander, Joseph C. <u>Manual of Traffic Engineer-ing Studies</u>. Institute of Transportation Engineers, Fourth Edition, 1976.
- 11. Baerwald, John E., Editor. <u>Transportation and Traffic Engineering</u>
 Handbook. Prentice Hall, Inc., Englewood Cliffs, New Jersey, 1976.

- 12. Alder, Henry L. and Roessler, Edward B. <u>Introduction to Probabil-ity and Statistics</u>. W. H. Freeman and Company, San Francisco, California, 1968.
- 13. Michaels, Richard M. "Two Simple Techniques for Determining the Significance of Accident-Reducing Measures." <u>Traffic Engineering</u>, Volume 36, No. 12, September, 1966, Alexandria, Virginia.
- 14. Gerlough, Daniel L. and Barnes, Frank C., <u>Poisson and Other Distributions in Traffic</u>. End Foundation for Transportation, Sagatuck, Connecticut, 1971.
- 15. Edwards, Allen L. Experimental Design in Psychological Research, 3rd Edition. Holt, Rinehart and Winston, Inc., New York, N.Y., 1968.
- 16. American Association of State Highway and Transportation Officials.

 A Manual on User Benefit Analysis of Highway and Bus-Transit

 Improvements. Washington, D.C., 1978.
- 17. Moss, James N. District Maintenance Engineer State Department of Highways and Public Transportation. Amarillo, Texas, Telephone Interview, 1978.
- 18. Paquette, Radnor J., Ashford, Norman, and Wright, Paul H. <u>Transportation Engineering</u>. The Ronald Press Company, New York, N.Y., 1972.
- 19. Curry, David A., and Anderson, Dudley G. "Procedures for Estimating Highway User Costs, Air Pollution and Noise Effects."
 NCHRP 133, Highway Research Board, 1972.

APPENDIX A

TRAVEL TIME DATA

TABLE A.1

NUMBER OF STOPS IN SIX RUNS

| | AM P | eak | Noon | Peak | PM P | eak | Off- | Peak |
|-------------|--------|--------|----------|---------|---------|---------|--------------|------------|
| | Before | After | Before | After | Before | After | Before | After |
| Adams | | | | | | | * | |
| NB | 7 | 1 0 | 9 | 5 13 | 10 9 | 19 8 | I.D.* | I.D. 12 |
| SB | Ь | U | 9 | 13 | 9 | 0 | 10 | 14 |
| Amar. Blvd. | | | | | | | | |
| EB | 5 2 | 0 0 | 2 1 | 0 1 | 5 2 | 12 1 | 0 | 0 0 |
| WB | 2 | U | _ | 1 | 2 | Ţ | | U |
| Buchanan | | | | | | | | |
| NB | 13 | 5 | 7 | 6 | 12 | 2 | 7 | 4 |
| Fillmore | | | | | | | | |
| NB | 7 | 5 | 14 | 1 | 9 | 4 | 7 | 7 |
| Pierce | | | | | | | | |
| SB | 6 | 6 | 13 | 5 | 19 | 7 | 8 | 9 |
| | | • | | _ | | | | |
| Taylor | | _ | | | 1.0 | | 10 | 10 |
| SB | 13 | 3 | 14 | 1 | 16 | 64 | 13 | 10 |
| Po1k | | | | | | | ! ! | |
| NB | 17 | 11 | 19 | 32 | 24 | 15 | 22 | 25 |
| SB | 25 | 22 | 26 | 22 | 29 | 21 | 25 | 25 |
| Tyler | | | | | | | | |
| NB | 16 | 12 | 12 | 11 | 12 | 9 | 21 | 7 |
| Harrison | | | <u> </u> | | | | 1 | |
| SB | 18 | 10 | 14 | 11 | 17 | 7 | 21 | 1 |
| | | | | | | | | |
| Van Buren | | _ | | • | | 7.0 | 07 | 00 |
| NB | 17 | 1 | 17 | 2 | 15 | 18 | 27 | 23 |
| Jackson | | | | | | | <u> </u> | |
| SB | 10 | 26 | 10 | 18 | 2 | 12 | 17 | 13 |

. . . .

TABLE A.1 (Continued)

| | AM P | eak | Noon | Peak | PM P | eak | Off- | Peak |
|------------|----------|----------|----------|--------------|----------|----------|----------|----------|
| | Before | After | Before | After | Before | After | Before | After |
| 3rd | | | | | | | | |
| EB WB | 10 18 | 16 17 | 22 12 | 13 14 | 22 20 | 20 14 | 19 18 | 15 15 |
| 6th | | | | | | | | |
| EB WB | 30 16 | 28 19 | 33 18 | 30 0 | 25 18 | 30 27 | 34 17 | 33 11 |
| 7th | | | | | | | | |
| EB | 21 | 16 | 25 | 9 | 32 | 17 | 25 | 7 |
| 8th | | | | | | | | |
| WB | 23 | 15 | 20 | 7 | 21 | 11 | 25 | 11 |
| 9th | | | | | | | | |
| EB | 28 | 23 | 27 | 18 | 26 | 22 | 24 | 5 |
| 10th | | | | | | | | |
| EB WB | 35 34 | 35 25 | 36 20 | 29 6 | 24 26 | 20 24 | 34 19 | 43 5 |
| 11th | | | | | | | | |
| EB | 18 | 23 | 7 | 15 | 13 | 26 | 13 | 19 |
| Washington | | | | | | | | |
| NB SB | 4 0 | 5 3 | 6 2 | 2 0 | 11 1 | 11 0 | 1 | 0 0 |
| Georgia | | | | | | | | |
| nb Sb | 15 9 | 0 2 | 20 14 | 13 1 | 17 14 | 14 5 | 15 10 | 0 5 |
| Western | | | | | | | | |
| NB SB | 5 4 | 0 | I.D. | I.D. I.D. | 2 5 | 4 5 | 4 2 | 6 |

^{*} Insufficient Data

TABLE A.2

NUMBER OF SECONDS OF DELAY IN 6 RUNS

| | AM I | ?eak | Noor | l Peak | PM F | ?eak | Off- | Peak |
|----------------|------------|------------|------------|------------|------------|------------|-------------|-------------|
| | Before | After | Before | After | Before | After | Before | After |
| Adams | | | | | | | * | |
| NB SB | 29 63 | 21 0 | 87 87 | 80 250 | 217 153 | 375 111 | 1.D. 128 | I.D. 219 |
| Amar. Blvd. | | | | | | | | |
| EB WB | 14 | 0 0 | 5 3 | 0 2 | 74 7 | 87 2 | 0 | 0 0 |
| Buchanan | | | | | | | | |
| NB | 263 | 143 | 145 | 139 | 252 | 8 | 116 | 141 |
| Fillmore NB | 181 | 96 | 210 | 34 | 154 | 21 | 222 | 122 |
| Pierce | | | | | | | | |
| SB | 114 | 52 | 221 | 57 | 327 | 36 | 69 | 137 |
| Taylor SB | 198 | 87 | 260 | 28 | 484 | 187 | 134 | 99 |
| Polk | | | | | | | | |
| NB SB | 229 358 | 151 406 | 297 500 | 509 281 | 322 443 | 355 426 | 473 341 | 240 340 |
| Tyler NB | 43 | 147 | 75 | 220 | 50 | 109 | 64 | 107 |
| Harrison | | | | | | | | |
| SB | 158 | 37 | 120 | 242 | 234 | 71 | 174 | 2 |
| Van Buren | | | | | | | | |
| NB | 116 | 4 | 90 | 49 | 148 | 188 | 96 | 46 |
| Jackson SB | 143 | 448 | 106 | 87 | 10 | 183 | 65 | 25 |

TABLE A.2 (Continued)

| AM P | eak | Noon | Peak | PM P | eak | Off- | Peak |
|------------|--|--|--|---|---|---|---|
| Before | After | Before | After | Before | After | Before | After |
| | | | | | | | |
| 160 269 | 380 533 | 204 155 | 95 77 | 247 284 | 665 424 | 255 283 | 231 138 |
| | | | | | | | |
| 599 346 | 604 325 | 562 357 | 654 0 | 495 401 | 632 577 | 840 445 | 636 284 |
| | | | | | | | |
| 219 | 242 | 329 | 44 | 566 | 561 | 204 | 171 |
| | | | | | | | |
| 519 | 419 | 388 | 82 | 441 | 226 | 473 | 97 |
| | | | | | | | |
| 220 | 345 | 339 | 602 | 267 | 657 | 550 | 53 |
| | | | | | | | |
| 743 | 639 | 716 | 475 | 611 | 463 | 1007 | 744 |
| 541 | 534 | 284 | 61 | 705 | 601 | 360 | 110 |
| | | | | | | | |
| 542 | 689 | 78 | 134 | 235 | 725 | 105 | 230 |
| | | | | | | | |
| 21 | 26 | 15 | 5 | 181 | 290 | 34 | 0 |
| U | 26 | 50 | O | 9 | O | 19 | 0 |
| | | | | | | | |
| 254 176 | 0 | 534 | 340 71 | 563 | 123 | 162 | 0 32 |
| 1/0 | . . | 204 | 11 | סטכ | 30 | 133 | 34 |
| | : | | | | | | |
| | 0 | | I.D. | 76 110 | 22 39 | 141 36 | 46 6 |
| | 160 269 599 346 219 519 220 743 541 542 | 269 533 599 604 346 325 219 242 519 419 220 345 743 639 541 534 542 689 21 26 0 26 254 0 176 9 | Before After Before 160 380 204 269 533 155 599 604 362 346 325 357 219 242 329 519 419 388 220 345 339 743 639 716 541 534 284 542 689 78 21 26 15 0 26 50 254 0 534 176 9 284 108 0 I.D. | Before After Before After 160 380 204 95 269 533 155 77 599 604 562 654 346 325 357 0 219 242 329 44 519 419 388 82 220 345 339 602 743 639 716 475 541 534 284 61 542 689 78 134 21 26 15 5 0 26 50 0 254 0 234 71 108 0 1.D. 1.D. | Before After After After After After After After After After After After After After | Before After Before After Before After 160 380 204 95 247 665 269 533 155 77 284 424 599 604 562 654 495 632 346 325 357 0 401 577 219 242 329 44 566 561 519 419 388 82 441 226 220 345 339 602 267 657 743 639 716 475 611 463 541 534 284 61 705 601 542 689 78 134 235 725 21 26 15 5 181 290 0 26 50 0 9 0 254 0 534 340 563 123 176 9 284 | Before After After Before After Af |

^{*} Insufficient Data

APPENDIX B COMPUTATION OF STOPS PER DAY

TABLE B.1
COMPUTATION OF STOPS PER DAY IN BEFORE AND AFTER PERIODS

| - | | | | | | | | Before | a | | | | | | | After | н | | | |
|----------------|------------|-----------|-------------------------------|-------------|----------------------|--------------|------------------|-------------|------------|--------------|--------------|-------------|------------|--------------|------------------|-------------|------------|--------------|------------|--------------|
| ; | | Vo. | Volume | | | St | Stops Vehicle | | | 200 | Stops Day | | | Veh | Stops Vehicle | | | Stops | 5d | |
| Street | AN Peak | | Noon PN Off Peak Peak Peak | Off Peak | AM Peak | Noon Peak | PM Peak | Off Peak | AM Peak | Noon Peak | 구속 | Off Peak | AM Peak | Noon Peak | PN Peak | Off Peak | AM Peak | Noon Peak | PN Peak | Off Peak |
| Adams NB | 1200 | 1200 700 | 650 | 5900 | 650 5900 1.167 1.500 | 1.500 | 1.667 | 1 | 1400 | 1050 | 1084 | 1 | 0.167 | 0.833 | 3.167 | 1 | 200 | .583 | 2059 | 1 |
| Adams SB | 200 | 200 | 950 | 3700 | 3700 1.000 1.500 | 1,500 | 1.500 | 1.667 | 200 | 750 | 1425 | 8919 | 0 | 2.167 | 1.333 | 2.000 | 0 | 1084 | 1266 | 2400 |
| Amar. Blvd. EB | . 650 | 750 | 1100 | 8100 | 8100 0.833 | 0.333 | 0.833 | 0 | 541 | 250 | 916 | • | 0 | 0 | 2.000 | 0 | 0 | 0 | 2200 | 0 |
| Amar. Blvd. WB | 550 | 550 | 750 | 2900 | 0.333 | 0.167 | 0.333 | 0 | 183 | 92 | 250 | 0 | 0 | 0.167 | 0.167 | 0 | 0 | 92 | 125 | 0 |
| Buchanan | 1700 | 1700 1100 | 1800 | 9400 | 2.167 | 1,167 | 2.000 | 1.167 | 3684 | 1284 | 3600 | 1469 | 0.833 | 1.000 | 0.333 | 0.667 | 9171 | 1100 | 9009 | 4,269 |
| Fillmore | 1050 | 950 | 950 | 9750 | 1.167 | 2.333 | 1.500 | 1.167 | 1225 | 2216 1 | 1425 1 | 11,378 | 0.833 | 0.167 | 0.667 | 1.167 | 875 | 159 | 969 | 11,378 |
| Pierce | 009 | 950 | 1600 | 8850 | 1.000 | 7,167 | 3.167 | 1.333 | 009 | 2059 | 5067 1 | 11,797 | 1.000 | 0.833 | 1.167 | 1.500 | • 600 | 791 | 1867 | 13,327 |
| Taylor | 650 | 950 | 1600 | 8450 | 2.167 | 2,333 | 2.667 | 2.167 | 1409 | 2216 | 4267 1 | 18,311 | 0.500 | 0.167 | 2,333 | 1.667 | 325 | 109 | 3733. | 3733. 14,086 |
| Polk NB | 150 | 300 | 400 | 1150 | 2.833 | 3,167 | 4.000 | 3.667 | 425 | 950 | 1600 | 4217 | 1.833 | 5,333 | 2.500 | 4.167 | 275 | 1600 | 1000 | 4792 |
| Polk SB | 150 | 300 | 400 | 1150 | 4.167 | 4,333 | 4.833 | 4.167 | 625 | 1300 | 1933 | 4792 | 3,667 | 3.667 | 3,400 | 4.167 | 550 | 1100 | 1400 | 4792 |
| Tyler | 150 | 250 | 200 | 3100 | 2.667 | 2.000 | 2.000 | 3.500 | 400 | 200 | 400 1 | 10,050 | 2.000 | 1.833 | 1.500 | 1.167 | 300 | 458 | 300 | 3617 |
| Harrison | 300 | 200 | 1100 | 3000 | 3.000 | 2.333 | 2,833 | 3.500 | 006 | 1167 | 3116 10 | 10,500 | 1.667 | 1.833 | 1.167 | 0.167 | 200 | 917 | 1283 | 501 |
| Van Buren | 200 | 100 | 100 | 1000 | 2.833 | 2,833 | 2.500 | 4.500 | 292 | 283 | 250 | 4500 | 0.167 | 0.333 | 3.000 | 3,833 | 33 | 33 | 30 | 3833 |
| Jackson | 100 | 350 | 650 | | 2600 1.667 | 1.667 | 0.333 | 2.833 | 167 | 583 | 216 | 7366 | 4.333 | 3.000 | 2.000 | 2.167 | 433 | 1050 | 1300 | 5634 |
| 3rd EB | 350 | 400 | 450 | 2900 | 2900 1.167 3.0 | 3.667 | 3.667 | 3.167 | 604 | 1467 | 1650 | 9184 | 2.667 | 2.167 | 3.333 | 2.500 | 933 | 867 | 1500 | 7250 |
| 3rd WB | 350 | 350 400 | 200 | 3000 | 500 3000 3.000 2.000 | 2.000 | 3,333 | 3.000 | 1050 | 800 | 1667 | 0006 | 2.833 | 2,333 | 2,333 | 2.500 | 885 | 933 | 1167 | 7500 |

TABLE B.1 (Continued)

| | | | | | | | | Before | re | | | | | | | After | 1: | | | |
|---------------|------------|--------------|----------------------|-------------|------------|--------------|------------------|-------------|------------|--------------|--------------|-------------|------------|-----------------|------------|-------------|------------|--------------|------------|--------------|
| | | Vol | Volume | | | St | Stops /ehicle | | | S | Stops Day | | | Stops Vehici | Stops | | | Stops | D 1 | |
| Street | AM Peak | Noon Peak | Noon PM Peak Peak | Off Peak | AM Peak | Noon Peak | PM Peak | Off Peak | AM Peak | Noon Peak | PM Peak | 0ff Peak | AM Peak | Noon Peak | PM Peak | Off Peak | AM Peak | Noon Peak | PN Peak | Off. Peak |
| 6th EB | 200 | 150 | 300 | 1150 | 5,000 | 5.500 | 4.167 | 5.667 | 100 | 825 | 1250 | 6517 | 4.667 | 5.000 | 5.000 | 5,500 | 933 | 750 | 1500 | 6325 |
| 6th WB | 300 | 009 | 200 | 4900 | 2.667 | 3.000 | 3.000 | 2.833 | 800 | 1800 | 1500 | 1500 13,882 | 3,167 | 0 | 4.500 | 1.833 | 950 | | 2250 | 8982 |
| 7th EB | 400 | 200 | 650 | 3550 | 3.500 | 4.167 | 5,333 | 4.167 | 1400 | 2084 | 3466 | 3466 14,793 | 2,667 | 1.500 | 2.833 | 1.167 | 1067 | 750 | 1841 | 4143 |
| 8th WB | 750 | 450 | 650 | 3550 | 3,833 | 3,333 | 3.500 | 4.167 | 2875 | 1500 | 2275 | 2275 14,793 | 2,500 | 1.167 | 1.833 | 1.833 | 1875 | 525 | 1191 | 6507 |
| 9th EB | 150 | 150 | 200 | 1500 | 4.667 | 4.500 | 4,333 | 4.000 | 700 | 675 | 867 | 0009 | 3,833 | 3,000 | 3.667 | 0.833 | 575 | 450 | 733 | 1250 |
| 10th EB | 200 | 250 | 350 | 2200 | 5.833 | 6.000 | 4.000 | 5.667 | 1167 | 1500 | 1400 | 12,467 | 5.833 | 4,833 | 3,333 | 7.167 | 1167 | 1208 | 1167 | 15,767 |
| 10th WB | 550 | 750 | 750 1050 | 6050 | 5.667 | 3,333 | 4,333 | 3.167 | 3117 | 2500 | 4550 | 4550 19,160 | 4.167 | 1.000 | 4.000 | 0.833 | 2292 | 750 | 4200 | 2040 |
| 11th EB | 200 | 250 | 400 | 1900 | 3.000 | 1.167 | 2,167 | 2.167 | 009 | 292 | 867 | 4117 | 3,833 | 2,500 | 4,333 | 3.167 | 167 | 625 | 1733 | 2109 |
| Washington NB | 650 | 200 | 650 | 0067 | 0.667 | 1,000 | 1.833 | 0.167 | 434 | 200 | 1191 | 818 | 0,833 | 0.333 | 1.833 | 0 | 541 | 167 | 1191 | 0 |
| Washington SB | 1350 | 900 | 950 | 8450 | 0 | 0.333 | 0.167 | 0.167 | 0 | 300 | 159 | 1411 | 0.500 | 0 | 0 | 0 | 675 | 0 | 0 | 0 |
| Georgia NB | 550 | 700 | 700 1000 | 0099 | 2,500 | 3,333 | 2.833 | 2.500 | 1375 | 2333 | 2833 | 16,500 | 0 | 2,167 | 2.333 | 0 | 0 | 1517 | 2333 | 0 |
| Georgia SB | 250 | 800 | 800 1200 | 0029 | 1,500 | 2,333 | 2,333 | 1.667 | 375 | 1866 | 2800 | 7819 | 0.333 | 0.167 | 0.833 | 0.833 | 83 | 134 | 1000 | 5581 |
| Western NB | 550 | 009 | 750 | 5550 | 0,833 | : | 0.333 | 0.667 | 458 | 1 | 250 | 3669 | 0 | ı | 0.667 | 1.000 | 0 | j | 200 | 5550 |
| Western SB | 550 | 750 | 750 1100 | 8150 | 0,667 | 1 | 0.833 | 0.333 | 367 | , | 916 | 2714 | 0 | | 0.833 | 0.167 | 0 | , | 916 | 1361 |

TABLE B.2

COMPILATION OF STOPS PER DAY BY SECTION AND FOR TOTAL SYSTEM IN BEFORE AND AFTER PERIODS

| | | Вє | fore | | | Af | ter | |
|-----------------|------------|--------------|------------|-------------|------------|--------------|------------|-------------|
| | | | ops ay | | | | ops ay | |
| Street | AM Peak | Noon Peak | PM Peak | Off Peak | AM Peak | Noon Peak | PM Peak | Off Peak |
| Sections 1 & 2 | • | | | | | | | |
| Buchanan | 3684 | 1284 | 3600 | 7464 | 1416 | 1100 | 600 | 4269 |
| Fillmore | 1225 | 2216 | 1425 | 11,378 | 815 | ~ 159. | 634 - | 11,378 |
| Pierce | 600 | 2059 | 5061. | 11,741 | 600 | 741 | 1867 | 13,275 |
| Taylor | 1404 | 2216 | 4267 | 18,311 | 325 | 109 | 3733 | 14,086 |
| Polk NB | 425 | 950 | 1600 | 4217 | 275 | 1600 | 1000 | 4742 |
| Polk SB | 625 | 1300 | 1433 | 4792 | 550 | 1100 | 1400 | 4792 |
| Tyler | 400 | 500 | 400 | 10,850 | 300 | 458 | 300 | 3617 |
| Harrison | 900 | 1167 | 3116 | 10,500 | 500 | 917 | 1283 | 501 |
| Van Buren | 567 | 283 | 250 | 4500 | 33 | 33 | 30 | 3833 |
| Jackson | 167 | 583 | 216 | 7366 | 433 | 1050 | 1300 | 5634 |
| 3rd EB | 408 | 1467 | 1650 | 9184 | 933 | 867 | 1500 | 7250 |
| 3rd WB | 1050 | 800 | 1667 | 9000 | 992 | 933 | 1167 | 7500 |
| 6th EB | 100 | 825 | 1250 | 6517 | 933 | 750 | 1500 | 6325 |
| 6th WB | 800 | 1800 | 1500 | 13,882 | 950 | 0 | 2250 | 8982 |
| 7th EB | 1400 | 2084 | 3466 | 14,793 | 1067 | 750 | 1841 | 4143 |
| 8th | 2875 | 1500 | 2275 | 14,745 | 1875 | 525 | 1191 | 6507 |
| 9th | 700 | 675 | 867 | 6000 | 575 | 450 | 733 | 1250 |
| 10th EB | 1167 | 1500 | 1400 | 12,467 | 1167 | 1208 | 1167 | 15,767 |
| 10th WB | 3117 | 2500 | 4550 | 19,168 | 2292 | 750 | 4200 | 5040 |
| llth EB | 600 | 292 | 867 | 4117 | 767 | 625 | 1733 | 6017 |
| Σ Section 1 & 2 | 22,219 | 26,001 | 41,366 | 201,101 | 16,858 | 14,175 | 29,429 | 174,958 |

TABLE B.2 (Continued)

| | | Be | fore | | | Af | ter | |
|--------------------|-------------|------|-----------|----------|----------|------|-----------|------|
| | | _ | ops ay | | | | ops ay | • |
| | AM | Noon | PM | Off | AM | Noon | PM | Off |
| Street | Peak | Peak | Peak | Peak | Peak | Peak | Peak | Peak |
| Section 3 | | | | | | | | |
| Amar. Blvd. EB | 541 | 250 | 916 | 0 | 0 | 0 | 2200 | 0 |
| Amar Blvd. WB | 183 | 92 | 250 | 0 | 0 | 92 | 125 | _ 0 |
| Σ Section 3 | 724 | 342 | 1166 | 0 | 0 | 92 | 2325 | 0 |
| | | | | | | | | |
| Section 4 | | | | | | | | |
| Adams NB | 1400 | 1050 | 1084 | _ | 200 | 583 | 2059 | _ |
| Adams SB | 200 | 750 | 1425 | 6168 | 0 | 1084 | 1266 | 7400 |
| Washington NB | 434 | 500 | 1191 | 818 | 541 | 167 | 1191 | 0 |
| Washington SB | 0 | 300 | 159 | 1411 | 675 | 0 | Q | O O |
| Σ Section 4 | 2034 | 2600 | 3859 | 8397 | 1416 | 1834 | 4516 | 7400 |
| | | | | | | | - | |
| Coopies E | | | | | | | | |
| Section 5 | | | | | _ | | | |
| Georgia NB | 1375 | 2333 | 2833 | 16,500 | 0 | 1517 | 2333 | 0 |
| Georgia SB | 375 | 1866 | 2800 | 7819 | 83 | 134 | 1000 | 5581 |
| Σ Section 5 | 1150 | 4199 | 5633 | 24,319 | 83 | 1651 | 3333 | 5581 |
| | | | | | | | | |
| Section 7 | | | | | | | | |
| Western NB | 458 | _ | 250 | 3669 | 0 | - | 500 | 5550 |
| Western SB | 367 | _ | 916 | 2714 | 0 | | 916 | 1361 |
| Σ Section 7 | 825 | - | 1166 | 6383 | 0 | - | 1416 | 6911 |
| | | | | | | | | |
| | <u> </u> | | <u> </u> | <u> </u> | <u> </u> | | <u> </u> | |

^{*} TOTAL SYSTEM Stops:

BEFORE - 354,084 AFTER - 271,978

TOTAL SYSTEM REDUCTION IN STOPS = $\frac{354,084 - 271,978}{354,084} = 23.2\%$

APPENDIX C

t-TEST ANALYSIS OF REDUCTION IN NUMBER OF STOPS BY INDIVIDUAL STREET AND DIRECTION

table c.1
t-Test analysis of reduction in stops for northbound adams street

| | <u></u> | · | | | |
|----------------|----------|------------------------|-----------------------|--------------------|---|
| TIME PERIOD | RUN # | STOPS BEFORE (B) | STOPS AFTER (A) | DIFF B-A (D) | REMARKS AND CALCULATIONS |
| AM | 1 | 2 | 0 | 2 | H _o : M _d =0 \bar{D} = 1 (One tailed $S_{\bar{d}} = \sqrt{0.4}$ |
| Peak | 2 | 1 | 0 | 1 | |
| | 3 | 1 | 0 | 1 | $S_{\overline{d}} = \sqrt{.0667} = .258$ $t = \frac{\overline{D} - 0}{S_{\overline{d}}} = \frac{1}{.258} = 3.88$ |
| • | 4 | 1 | 1 | 0 | v = 5 |
| | 5 | 1 | 0 | 1 | t _{.05} = 2.015 |
| | 6 | 1 | 0 | 1 | ·• Reject H _o |
| Noon | 1 | 0 | 1 | -1 · | SD = 4 |
| Peak | 2 | 3 | 2 | 1 | D = .667 |
| | 3 | - 1 | 0 | | $S_{\overline{a}} = \sqrt{1.0667}$ |
| | 4 | 1 | . 1 | 0 | $S_{d} = \frac{\sqrt{1.0667}}{\sqrt{6}} = \sqrt{.1778} = .4216$ |
| | 5 | . 2 | 0 | 2 | $t = \frac{.667-0}{.4216} = 1.58; t_{0.5} = 2.015$ |
| | 6 | 2 | 1 | 1 | .Accept Ho |
| • | | | | ٠. | |
| PM Peak | 1 | 1 | 2 | -1 | |
| 1 Cak | 2 | 1 | 3 | -2 | $\bar{D} = -1.5$ |
| | 3 | 2 . | 5 | -3 | $S_{d} = .4281$ |
| | 4 | . 2 | 3 | -1 | $t = \frac{1.5}{.4281} = 3.50$ |
| | 5 | 1 | 3 | -2 | •• Reject H _o |
| | 6 | 3 | 3 | 0 | |
| Off Peak | - | | | | |
| | | | - | | INCOMPLETE |
| | | | | | |

TABLE C.2

tTEST ANALYSIS OF REDUCTION IN STOPS FOR SOUTHBOUND ADAMS STREET

| TIME PERIOD | RUN # | STOPS BEFORE (B) | STOPS AFTER (A) | DIFF B-A (D) | REMARKS AND CALCULATIONS |
|----------------|----------|------------------------|-----------------------|--------------------|--|
| AM Do-slo | 1 | 1 | 0 | 1 | $\overline{D} = 1$ |
| Peak | 2 | 1 | 0 | 1 | S _d = 0 |
| | 3 | 1 | 0 | 1 | s _d = 0 |
| *: | 4 | 1 | 0 | 1 | $t = \frac{1-0}{0} = \infty > t_{.05}$ (2.015) |
| | 5 | 1 | 0 - | 1 | Reject H |
| | 6 | 1 | 0 | 1 | Reject no |
| : Noon | 1 | 3 | 2 | 1 | $\bar{D} =6667$ Accept H |
| Peak | 2 | 1 | 2 | -1 | o modely no |
| | 3 | 1 | -2 | -1 | |
| • | 4 | . 1 | 2 | -1 | |
| | 5 | 2 | 2 | | |
| | | | | 0 | |
| | 6 | 1 | 3 | -2 | |
| PM Peak | 1 | 2 | 1 | 1 | $\bar{D} = .16667$ Accept H _o |
| reak | 2 | 0 | 1 | -1 | |
| | 3 | 2 | 3 | -1 | |
| | 4 | o | 1 | -1 | |
| ٠. | 5 | 2 | 1 | 1 | |
| | . 6 | 3 | 1 | 2 | |
| • | | | | · ! | |
| Off Peak | 1 | 2 | 2 | 0 | $\overline{D} =3333$ Accept H _o |
| | 2 | 3 | 2 - | 1 | |
| <u>.</u> | 3 | 2 . | 2 | ٥. | · |
| , | 4 | . 1 | 2 | -1 | |
| | 5 | 1 | · 2 | -1 . | |
| | 6 | 1 | 2 | -1 | |

t-TEST ANALYSIS OF REDUCTION IN STOPS FOR EASTBOUND 10th STREET

| | | · | | | |
|----------------|----------|------------------------|-----------------------|--------------------|--------------------------------------|
| TIME PERIOD | RUN # | STOPS BEFORE (B) | STOPS AFTER (A) | DIFF B-A (D) | REMARKS AND CALCULATIONS |
| AM Peak | | | | | |
| | | | | | INCOMPLETE |
| | | | | | |
| Noon Peak | 1 | 4 | 4 | 0 | D = 1.16 |
| reak | 2 | 7 | 5 | 2 | S _t = .477 |
| | 3 | 7 | 4 | 3 | t = 2.44 > t _{.05} (2.015) |
| | 4 | 7 | 6 | 1 | Reject H |
| | 5 | 5 | . 5 | 0 | |
| | 6 | 6 | 5 | 1 | |
| PM | 1 | 6 | 3 | 3 | D = .667 |
| Peak | 2 | 4 | 4 . | 0 | $S_{\overline{d}} = .494$ |
| | 3 | 3 | 3 | 0 | t = 1.348 < t _{.05} (2.015) |
| | 4 | 4 | 4 | 0 | Accept H _o |
| | 5 | 3 | 3 | 0 | |
| • | · 6 | 4 | 3 | 1 | |
| Off Peak | • | | | | |
| i | | | | - | INCOMPLETE |
| | | | · | | |
| | | L | | | |

table c.4 table c.4 table c.4

| TIME PERIOD | RUN # | STOPS BEFORE (B) | STOPS AFTER (A) | DIFF B-A (D) | REMARKS AND CALCULATIONS |
|----------------|----------|------------------------|-----------------------|--------------------|--------------------------------|
| AM Peak | 1 | 5 | 6 | -1 | D = 1.5 |
| reak | 2 | 6 | 6 | 0 | S _d = .846 |
| | 3 | 5 | 4 | 1 | t = 1.77 Accept H _o |
| • | 4 | 7 | 5 | 2 | |
| | 5 | 5 | 3 | 2 | |
| | 6 | 6 | 1 | 5 | |
| PM | 1 | 4 | 1 | 3 | $\overline{D} = 2.33$ |
| Peak | 2 | 4 | 0 | 4 | $S_{\overline{d}} = .714$ |
| | 3 | 2 | 3 | -1 | t = 3.26 Reject H _o |
| | 4 | . 4 | . 1 | 3 | |
| | 5 | 4 | 1 | 3 | |
| | 6 | 2 | 0 | 2 | |
| Noon | 1 | 4 | 4 | 0 | $\vec{D} = .333$ |
| Peak | 2 | 4 | 3 | 1 | $S_{\overline{d}} = .333$ |
| . | 3 | 4 | 3 | 1 | t = 1 Accept H |
| | 4 | . 5 | 6 | -1 | |
| ٠. | 5 | 5 | 4 | 1 | |
| | . 6 | 4 | 4 | . 0 | |
| Off | 1 | 4 | 1 | 3 | $\overline{D} = 2.33$ |
| Peak | 2 | 3 | 1 | 2 | $S_{\overline{d}} = .714$ |
| | 3 | 4 | 0 , | · 4 | $t = 3.26 > t_{.05} (2.015)$ |
| | 4 | 4 | 1 | 3 | Reject H |
| | 5 | 5 | · 2 | 3 | 0 |
| | 6 | 0. | 1 | -1 | |

| TIME PERIOD | RUN # | STOPS BEFORE (B) | STOPS AFTER (A) | DIFF B-A (D) | REMARKS AND CALCULATIONS |
|----------------|----------|------------------------|-----------------------|--------------------|---------------------------|
| AM Peak | 1 | 3 | 4 | -1 | D =333 |
| reak | 2 | 3 | 4 | -1 | $s_{\overline{d}} = .714$ |
| | 3 | 3 | 4 | -1 | t =466 Accept H |
| • | 4 | 1 | 4 | 3 | |
| | 5 | 2 | 4 | -2 | |
| | 6 | 3 | 3 | 0 | |
| Noon | 1 | 1 . | 3 | -2 | D̄ = −1.33 |
| Peak | 2 | 1 | 2 | -1 | $S_{\overline{d}} = .333$ |
| | 3 | 1 | .3 | -2 | $t = -4$ Accept H_0 |
| | 4 | 1 | 3 | -2 | |
| | 5 | 1 | 2 | -1 | · |
| • | 6 | 2 | 2 | 0 | • |
| PM | 1 | 3 | 3 | 0 | D = -2.16 |
| Peak | 2 | 2 | 5 | -3 | $S_{\overline{d}} = .477$ |
| • | 3 | 1 . | 4 | -3 | t = -4.539 Accept H |
| | 4 | 1 | 4 | -3 | · |
| | 5 | 3 | 5 | -2 | |
| | 6 | 3 | 5 | -2 | · |
| Off | 1 | 1 | 2 | -1 | D =833 |
| Peak | 2 | 1 | 4 - | -3 | $S_{\overline{d}} = .792$ |
| | 3 | 3 | 3 | 0 . | t = -1.05 Accept H |
| • - | 4 | 3 | 1 | 2 | |
| | 5 | 4 | 4 | 0 . | |
| | 6 | 1 | 4 | -3 | |

table c.6
t-test analysis of reduction in stops for Eastbound ama boulevard

| TIME PERIOD | RUN | STOPS BEFORE (B) | STOPS AFTER (A) | DIFF B-A (D) | . REMARKS AND CALCULATIONS |
|----------------|-----|------------------------|-----------------------|--------------------|------------------------------|
| AM | 1 | 1 | 0 | 1 | $\overline{D} = .8333$ |
| Peak | 2 | 1 | 0 | 1 | s _d = .16667 |
| | 3 | 1 | 0 | 1 | $t = 5.00 > t_{.05} (2.015)$ |
| • | 4 | o | 0 | 0 | Reject H _o |
| | 5 | 1 | 0 | 1 | |
| | 6 | 1 | 0 | 1 | |
| Noon | 1 | 0 | _ 0 | 0 | $\bar{D} = .3333$ |
| Peak | 2 | o | 0 | 0 | $s_{\overline{d}} = .2108$ |
| • | 3 | . 1 | 0 | 1 | t = 1.58 Accept H |
| • | 4 | o | Q | 0 | |
| | 5 | o | 0 | 0 | |
| | 6 | 1 | 0 | ı | |
| PM | 1 | 0 | 2 | -2 | $\bar{D} = -1.16667$ |
| Peak | 2 | 2 | 1 . | 1 | $S_{\overline{d}} = .543$ |
| | 3 | 1 | 2 | -1 | t = -2.15 Accept H |
| | 4 | 0 | 3 | -3 | • |
| | 5 | 1 | 2 | -1 | • |
| | . 6 | 1 | 2 | -1 | |
| Off | 1 | o | o | 0 | t = 0 Accept H |
| Peak | 2 | o | 0 | 0 | Ů |
| | 3 | o | 0 | 0. | |
| | 4 | 0 | 0 | 0 | |
| | 5 | 0 | 0 | 0 | |
| | 6 | ó, | 0 | 0 | |

TABLE C.7
t-TEST ANALYSIS OF REDUCTION IN STOPS FOR WESTBOUND AMA BOULEVARD

| TIME PERIOD | RUN # | STOPS BEFORE (B) | STOPS AFTER (A) | DIFF B-A (D) | REMARKS AND CALCULATIONS |
|----------------|----------|------------------------|-----------------------|--------------------|--------------------------------|
| AM Peak | 1 | 0 | 0 | 0 | $\overline{D} = .3333$ |
| reak | 2 | 0 | 0 | 0 | $S_{\bar{d}} = .2108$ |
| | 3 | 0 | o | 0 | t = 1.58 Accept H _o |
| • | 4 | 1 | 0 | 1 | |
| : | 5 | 1 | 0 | 1 | |
| | 6 | 0 | 0 | 0 | |
| Noon Peak | 1 | 0 | 0 | 0 . | $\overline{D} = 0$ |
| | 2 | 0 | 0 | 0 | $S_{\overline{d}} = .2582$ |
| | 3 | 0 | 0 | 0 | t = 0 Accept H |
| | 4 | 1 | . 0 | 1 | |
| ; | 5 | . 0 | 1 | -1 | |
| • | 6 | 0 | 0 | 0 | |
| PM Peak | 1 | 0 | 0 | 0 | D = .16667 |
| ICAN | 2 | 0 | 1 | -1 | $S_{\overline{d}} = .3073$ |
| | 3 | 1 . | 0 | 1 | t = .542 Accept H _o |
| • | 4 | . 1 | .0 | 1 | |
| | 5 | 0 | 0 | 0 | |
| | 6 | 0 | 0 | 0 | |
| Off | 1 | 0 | 0 | 0 | t = 0 Accept H _o |
| Peak | 2 | 0 . | 0 | 0 | |
| | 3 | 0 | 0 | . 0 | |
| | 4 | 0 | 0. | 0 | |
| | 5 | 0 | 0 | 0 | |
| • | 6 | 0. | 0 | 0 | |

table c.8 table c.8 table c.8

| TIME PERIOD | RUN # | STOPS BEFORE (B) | STOPS AFTER (A) | DIFF B-A (D) | REMARKS AND CALCULATIONS |
|----------------|----------|------------------------|-----------------------|--------------------|---------------------------------|
| AM Peak | 1 | 4 | 1 | 3 | D = 1.333 |
| reak | 2 | 3 | 1 | 2 | $S_{\overline{d}} = .494$ |
| | 3 | 2 | 0 | 2 | t = 2.70 Reject H |
| | 4 | 1 | 1 | 0 | |
| • | 5 | 2 | 1 | 1 | |
| | 6 | 1 | 1 | 0 | |
| Noon | 1 | 2 | 1 | 1 | $\bar{D} = .1667$ |
| Peak | 2 | 1 | 1 | 0 | .S _d = .3073 |
| | 3 | 0 | .i | -1 | t = .542 Accept H _o |
| | 4 | 2 | 1 | 1 | |
| | 5 | 1 | 1 | 0 | |
| • | 6 | 1 | 1 | 0 | |
| PM | 1 | 1 | 0 | 1 | $\bar{D} \approx 1.6667$ |
| Peak | 2 | 2 | 0 | 2 | $S_{\overline{d}} = .558$ |
| | 3 | 1 . | 0 | 1 | t - 2.99 Reject H |
| | 4 | 4 | 0 | 4 | |
| | 5 | 3 | 1 | 2 | |
| | 6 | 1 | 1 | 0 | · |
| Off | 1 | 1 | 0 | 1 | $\bar{\mathbf{D}} = 0.5$ |
| Peak | 2 | 1 | 0 - | 1 | $S_{\overline{d}} = 0.619$ |
| | 3 | 1 | 2 | -1 | t = 0.808 Accept H _o |
| | 4 | 3 | 0 | 3 | |
| | 5 | o | 1 | -1 | • |
| • | 6 | 1 | 1 | 0 | |

t-TEST ANALYSIS OF REDUCTION IN STOPS FOR NORTHBOUND FILLMORE STREET

| TIME PERIOD | RUN # | STOPS BEFORE (B) | STOPS AFTER (A) | DIFF B-A (D) | REMARKS AND CALCULATIONS |
|----------------|----------|------------------------|-----------------------|--------------------|---------------------------------|
| AM | 1 | 3 | 1 | 2 | $\bar{D} = 0.3333$ |
| Peak | 2 | 1 | 0 | 1 | $S_{\overline{d}} = 0.494$ |
| | 3 | 1 | 2 | -1 | t = 0.674 Accept H _o |
| | 4 | 0 | 1 | -1 | |
| | 5 | 1 | 1 | 0 | |
| | 6 | 1 | 0 | 1 | |
| Noon | 1 | 2 | 0 | 2 | $\bar{D} = 2.1667$ |
| Peak | 2 | 2 | 0 | 2 | $.S_{\overline{d}} = 0.703$ |
| | 3 | 3 | 0 | 3 | t = 3.081 Reject H _o |
| | 4 | 5 | 0 | 5 | |
| | 5 | 1 | 1 | 0 | |
| • | 6 | 1 | 0 | 1 | |
| PM | 1 | 0 | 1 | -1 | $\bar{D} = 0.8333$ |
| Peak | 2 | 4 | ο . | 4 | $S_{\overline{d}} = .703$ |
| | 3 | 1 | 0 | 1 | t = 1.185 Accept Ho |
| | 4 | 1 | 1 | 0 | |
| | t | 2 | 1 | 1 | |
| | . 6 | 1 | 1 | 0 | |
| Off | 1 | 1 | 2 | -1 | $\overline{D} = 0$ |
| Peak | 2 | 1 | 0 | 1 | $S_{\overline{d}} = .365$ |
| | . 3 | 1 | 1 | 0 . | t = 0 Accept H _o |
| | 4 | 1 | 2 | -1 | |
| | 5 | 1 | 0 | 1 | |
| | 6 | 2 | 2 | 0 | |

t-TEST ANALYSIS OF REDUCTION IN STOPS FOR SOUTHBOUND PIERCE STREET

| TIME PERIOD | RUN # | STOPS BEFORE (B) | STOPS AFTER (A) | DIFF B-A (D) | REMARKS AND CALCULATIONS |
|----------------|----------|------------------------|-----------------------|--------------------|----------------------------------|
| AM | 1 | 3 | 0 | 3 | $\bar{\mathbf{D}} = 0$ |
| Peak | 2 | 0 | 1 | -1 | $S_{\bar{d}} = 0.730$ |
| | 3 | 0 | 2 | -2 | t = 0 Accept H _o |
| | 4 | 1 | О | 1 | · |
| | 5 | 1 | 1 | 0 | |
| | 6 | 1 | 2 | -1 | |
| Noon | 1 | 3 | 0 | 3 · | $\widetilde{D} = 1.3333$ |
| Peak | 2 | 0 | 0 | 0 | $s_{\overline{d}} = 0.558$ |
| | 3 | · 1 | О | 1 | t = 2.390 Reject H _o |
| | 4 | 1 | 1 | 0 | |
| | 5 | 5 | 2 | 3 | |
| | 6 | 3 | 2 | · 1 | |
| PM | 1 | | 1 | | |
| Peak | 2 | | 1 | | |
| | 3 | | 1 | | PM Peak Data Incomplete |
| | 4 | | 1 | | rm reak bata incomplete |
| | 5 | | 2 | | |
| | 6 | | 1 | | |
| Off | 1 | 1 | 1 | 0 | D = -0.16667 |
| Peak | 2 | 2 | 1 | 1 | $S_{\overline{d}} = 0.477$ |
| | 3 | 1. | 2 | · -1 | t = -0.349 Accept H _O |
| | 4 | 0 , | 2. | -2 | |
| | 5 | 2 | 2 | 0 | |
| | 6 | Ź | 1 | 1 | • |

TABLE C.11
t-TEST ANALYSIS OF REDUCTION IN STOPS FOR SOUTHBOUND TAYLOR STREET

| TIME PERIOD | RUN # | STOPS BEFORE (B) | STOPS AFTER (A) | DIFF B-A (D) | REMARKS AND CALCULATIONS |
|----------------|----------|------------------------|-----------------------|--------------------|---------------------------------|
| AM | 1 | 1 | 1 | 0 | D = 1.66667 |
| Peak | 2 | 2 | 0 | 2 | $S_{\overline{d}} = .422$ |
| | 3 | 2 | 0 | 2 | t = 3.953 Reject H _o |
| | 4 | 3 | 1 | 2 | |
| | 5 | 2 | 1 | 1 | |
| | 6 | 3 | 0 | 3 | |
| Noon | 1 | 2 | 0 | 2 | D = 2.16667 |
| Peak | 2 | 2 | 0 | 2 | $s_{\overline{d}} = 0.307$ |
| | 3 | . 2 | .0 | 2 | t = 7.050 Reject Ho |
| | 4 | 3 | 0 | 3 | |
| | 5 | 4 | 1 | 3 | |
| | 6 | 1 | . 0 | 1 | |
| PM Peak | 1 | 3 | 2 | 1 | $\overline{D} = 0.3333$ |
| reak | 2 | 3 | 2 | 1 | $s_{\bar{d}} = 0.333$ |
| | 3 | 2 | 2 | 0 | t = 1.00 Accept H |
| | 4 | 4 | 4 | 0 | |
| | 5 | 2 | 3 | -1 | · ··-·· |
| | 6 | 2 | 1 | 1 | • |
| Off | 1 | 0 | 1 | -1 | $\overline{D} = 0.5$ |
| Peak | 2 | 4 | 1 - | 3 | $S_{\overline{d}} = 0.806$ |
| | 3 | 0 | 1 | -1 . | t = 0.620 Accept H _o |
| • | 4 | 1 | 1 | 0 | |
| | 5 | 6 | 3 | 3 . | |
| | 6 | 2. | 3 | -1 | |

t-Test analysis of reduction in stops for northbound polk street

| | | | | | |
|----------------|----------|------------------------|-----------------------|--------------------|---------------------------------|
| TIME PERIOD | RUN # | STOPS BEFORE (B) | STOPS AFTER (A) | DIFF B-A (D) | REMARKS AND CALCULATIONS |
| AM | 1 | 3 | 3 | 0 | D = 1 |
| Peak | 2 | 4 | 1 | 3 | $S_{\overline{d}} = .683$ |
| | 3 | 1 | 1 | 0 | t = 1.464 Accept H _o |
| | 4 | 2 | 1 | 1 | |
| i | 5 | 5 | 2 | 3 | |
| , | 6 | 2 | 3 | -1 | |
| Noon | . 1 | 4 | 5 | -1 | $\overline{D} = -2.17$ |
| Peak | 2 | 2 | 6 | -4 | $S_{\overline{d}} = .477$ |
| | 3 | 4 | 5 | -1 | $t = -4.54$ Accept H_0 |
| | 4 | 3 | 5 | -2 | |
| | 5 | 3 | 6 | -3 | |
| • | 6 | 3 | 5 | -2 | |
| PM | 1 | 5 | 3 | 2 | $\overline{D} = 1.5$ (Sto 1) |
| Peak | 2 | 3 | 3 . | 0 | s _ā = .5 |
| | 3 | 6 . | 3 | 3 | t = 3 Reject H _o |
| • | 4 | 2 | 2 | 0 | |
| | 5 | 3 | 1 | 2 | |
| | . 6 | 5 | 3 | 2 | · |
| Off | 1 | 5 | 3 | 2 | $\bar{D} = .33$ |
| Peak | 2 | 5 | 5 | 0 | $S_{\overline{d}} = .421$ |
| | 3 | 5 . | 4 | 1. | t = .790 Accept H _o |
| | 4 | 3 | 4 | -1 | |
| | 5 | 4 | 4 | 0 | |
| | 6 | 5. | 5 | 0 | · |

TABLE C.13
t-TEST ANALYSIS OF REDUCTION IN STOPS FOR SOUTHBOUND POLK STREET

| TIME PERIOD | RUN # | STOPS BEFORE (B) | STOPS AFTER (A) | DIFF B-A (D) | REMARKS AND CALCULATIONS |
|----------------|----------|------------------------|-----------------------|--------------------|---------------------------------|
| AM | 1 | 6 | 5 | 1 | D = 0.5 |
| Peak | 2 | 4 | 5 | -1 | $S_{\overline{d}} = 0.671$ |
| | 3 | 3 | 5 | -2 | t = 0.745 Accept H _o |
| | 4 | 4 | 3 | 1 | |
| | 5 | 4 | 2 | 2 | |
| | 6 | 4 | 2 | 2 | |
| Noon | 1 | 3 | 5 | -2 · | $\bar{D} = 0.66667$ |
| Peak | 2 | 3 | 3 | 0 | $.s_{\overline{d}} = 0.615$ |
| | 3 | 6 | 5 | 1 | t = 1.085 Accept H _o |
| | 4 | 6 | . 4 | 2 | |
| | 5 | . 5 | 3 | 2 | |
| • | 6 | 3 | 2 | 1 | |
| PM | 1 | 4 | 4 | 0 | D = 1.5 |
| Peak | 2 | 6 | 4 | 2 | $s_{\overline{d}} = 0.563$ |
| | 3 | 6 · | 3 | 3 | t = 2.666 Reject H _o |
| | 4 | . 3 | . 3 | 0 | |
| | 5 | 5 | 4 | 1 | |
| , | 6 | 6 | 3 | 3 | |
| Off | 1 | 6 | 6 | 0 | $\bar{D} = 0$ |
| Peak | 2 | 4 | 7 | - 3 | $S_{\overline{d}} = 0.856$ |
| | . 3 | 6 . | 5 | · 1. | t = 0 Accept H _o |
| | 4 | 5 | 3. | 2 | |
| | 5 | 1 | 3 | -2 | |
| | 6 | 3 | 1 | 2 | |

TABLE C.14
t-TEST ANALYSIS OF REDUCTION IN STOPS FOR NORTHBOUND TYLER STREET

| TIME PERIOD | RUN Ø | STOPS BEFORE (B) | STOPS AFTER (A) | DIFF B-A (D) | REMARKS AND CALCULATIONS |
|----------------|----------|------------------------|-----------------------|--------------------|--------------------------------|
| AM | 1 | 3 | 2 | 1 | $\overline{D} = .667$ |
| Peak | 2 | 3 | 3 | 0 | $S_{\overline{d}} = .615$ |
| | 3 | 4 | 2 | 2 | t = 1.08 Accept H |
| | 4 | 3 | 2 | 1 | |
| | 5 | 3 | 1 | 2 | |
| | 6 | 0 | 2 | -2 | |
| Noon | 1 | 2 | 2 | 0 | D = .167 |
| Peak | 2 | 3 | 3 | 0 | $.S_{\overline{d}} = .307$ |
| | 3 | 2 | -1 | 1 | t = .542 Accept H |
| | 4 | 2 | 2 | 0 | |
| | 5 | 1 | 2 | -1 | |
| • | 6 | 2 | 1 | 1 | |
| PM | 1 | | 1 | | |
| Peak | 2 | | 1 | | |
| | 3 | | 2 | | |
| . • | 4 | | 2 | | PM Peak Data Incomplete |
| | 5 | | 1 | | |
| | 6 | | 2 | | |
| Off | 1 | 4 | 0 | 4 | $\overline{D} = 2.33$ |
| Peak | 2 | 4 | 1. | 3 | $S_{\overline{d}} = .494$ |
| | . 3 | 2 | 1 | 1. | t = 4.72 Reject H _o |
| • | 4 | 5 | 2 | 3 | |
| | 5 | 3 | 1 | 2 . | |
| | 6 | 3 | 2 | ı | |

t-TEST ANALYSIS OF REDUCTION IN STOPS FOR SOUTHBOUND HARRISON STREET

| TIME PERIOD | RUN # | STOPS BEFORE (B) | STOPS AFTER (A) | DIFF B-A (D) | . REMARKS AND CALCULATIONS |
|----------------|----------|------------------------|-----------------------|--------------------|--------------------------------|
| AM | 1 | 3 | 2 | 1 | D = 1.33 |
| Peak | 2 | 2 | 2 | 0 | $S_{\overline{d}} = .421$ |
| ı | 3 | 3 | 1 | 2 | t = 3.16 Reject H _o |
| | 4 | 3 | 2 | · 1 | |
| | 5 | 3 | 2 | 1 | · |
| į | 6 | 4 | 1 | 3 | |
| Noon | 1 | 3 | 2 | 1 | D = .5 |
| Peak | 2 | 2 | 3 | -1 | .S _d = .428 |
| : | 3 | 2 | 1 | 1 | t = 1.17 Accept H _o |
| | 4 | 3 | 1 | 2 | |
| | 5 | . 2 | 2 | 0 | |
| - | 6 | 2 | 2 | 0 | |
| PM | 1 | 3 | 0 | 3 | $\widetilde{D} = 1.67$ |
| Peak | 2 | 1 | 1 . | 0 | $S_{\overline{d}} = .083$ |
| | 3 | 3 . | 4 | -1 | t = 2.08 Reject H _o |
| • [| 4 | 2 | 1 | ı | |
| | 5 | 4 | 1 | 3 | |
| | 6 | 4 | 0 | 4 | |
| Off Peak | 1 | 3 | . 0 | 3 | D = 3.33 |
| reak | 2 | 4 | 0 | 4 | s _d = .33 |
| | 3 | 3 . | 1 | 2 . | t = 1.0 Reject H _o |
| | 4 | 3 | 0 | 3 | |
| | 5 | 4 | 0 | 4 | |
| | 6 | 4 . | 0 | 4 | |

table C.16 table c.16

| TIME PERIOD | RUN # | STOPS BEFORE (B) | STOPS AFTER (A) | DIFF B-A (D) | REMARKS AND CALCULATIONS |
|----------------|----------|------------------------|-----------------------|--------------------|----------------------------------|
| AM | 1 | 4 | 0 | 4 | D = 2.67 |
| Peak | 2 | 2 | 1 | 1 | $S_{\overline{d}} = .494$ |
| | 3 | 2 | 0 | 2 | t = 5.39 Reject H _o |
| | 4 | 3 | 0 | 3 | |
| | 5 | 2 | 0 | 2 | |
| | 6 | 4 | 0 | 4 | |
| Noon | 1 | 4 | 0 | 4 . | $\bar{D} = 2.5$ |
| Peak | 2 | 3 | 0 | . 3 | $S_{\bar{d}} = .619$ |
| | 3 | 2 | 0 | 2 | t = 4.04 Reject H _o |
| | 4 | 2 | . 0 | 2 | |
| | 5 | 4 | 0 | 4 | |
| | 6 | 2 | . 2 | 0 | |
| | | | | | · |
| PM Peak | 1 | 2 | 4 | -2 | $\bar{D} = -0.5$ |
| | 2 | 3 | 3 | 0 | $S_{\overline{d}} = .619$ |
| | 3 | 2 | 3 | -1 | t = -0.808 Accept H _o |
| | 4 | . 3 | 3 | 0 | |
| | 5 | 1 | 3 | -2 | |
| | 6 | 4 | 2 | . 2 | |
| Off | 1 | 3 | 4 | -1 | $\bar{D} = 0$ |
| Peak | 2 | 5 | 4 | 1 | $S_{\overline{d}} = .258$ |
| | . 3 | 3 | 3 | . 0 | t = 0 Accept H _o |
| | 4 | 4 | 4. | 0 | Ü |
| | 5 | 4 | 4 | 0 | |
| | 6 | 4 | 4 | 0 | |

table C.17 . table c.17 . table c.17

| TIME PERIOD | RUN # | STOPS BEFORE (B) | STOPS AFTER (A) | DIFF B-A (D) | REMARKS AND CALCULATIONS |
|----------------|----------|------------------------|-----------------------|--------------------|---------------------------------|
| AM | 1 | 2 | 5 | -3 | D = -2.67 |
| Peak | 2 | 2 | 3 | -1 | S _d = .557 |
| | 3 | 2 | 5 | -3 | t = -4.78 Accept H _o |
| ; | 4 | 1 | 5 | -4 | |
| ' | 5 | 2 | 3 | -1 | |
| | 6 | 1 | 5 . | -4 | |
| Noon Peak | 1 | 3 | 3 | o | D = -1.33 |
| reak | 2 | 3 | 3 | ó | $S_{\overline{d}} = .421$ |
| | 3 | 1 | -3 | -2 | t = -3.16 Accept H _o |
| | 4 | 1 | 3 | -2 | |
| | 5 | 1 | 3 | -2 | |
| | 6 | 1 | 3 | -2 | |
| PM Peak | 1 | 0 | 1 | -1 | D = -1.67 |
| reak | 2 | 0 | 2 | -2 | $S_{\overline{d}} = .210$ |
| | 3 | . 1 | 2 | -1 | t = -7.91 Accept H |
| | 4 | 1 | 3 | -2 | · |
| • | 5 | 0 | 2 | -2 | |
| | · 6 | 0 | 2 | -2 | |
| Off | 1 | 1 | 2 | -1 | D̄ = .333 |
| Peak | 2 | 2 | 2 - | 0 | $s_{\overline{d}} = .333$ |
| | 3 | 3 . | 2 | 1. | t = 1 Accept H |
| | 4 | 2 | 2 | 0 | |
| | 5 | 3 | · 2 | 1 . | |
| | 6 | 4. | 3 | 1 | |

TABLE C.18

TABLE C.18

TABLE C.18

| TIME PERIOD | RUN | STOPS BEFORE (B) | STOPS AFTER (A) | DIFF B-A (D) | REMARKS AND CALCULATIONS |
|----------------|-----|------------------------|-----------------------|--------------------|--------------------------------|
| | 1 | 1 | 1 | 0 | D =167 |
| AM Peak | 2 | o | 1 | -1 | s _a = .307 |
| | 3 | 0 | 1 | -1 | t =542 Accept H |
| | 4 | 1 | 1 | 0 | |
| | 5 | 1 | 0 | 1 | |
| | 5 | 1 | 1 . | 0 | |
| 27 | 1 | 1 | 0 | 1 | D = .667 |
| Noot Peak | 2 | 1 | 0 | 1 | $S_{\overline{d}} = .210$ |
| | 3 | 1 | 1 | 0 | t = 3.16 Reject H _o |
| • | 4 | 1 | 1 | 0. | |
| | 5 | 1 | o | 1 | |
| | 6 | 1 | 0 | 1 | |
| PK : | 1 | 1 | 1 | 0 | $\overline{D} = 0$ |
| Peźk | | 0 | 2 . | -2 | $S_{\overline{d}} = .516$ |
| | 3 | 3 · | 2 | 1 | t = 0 Accept H _o |
| | 4 | 1 | 2 | -1 | |
| | 5 | 3 | 2 | 1 | |
| | . 6 | 3 | 2 | . 1 | |
| · off | 1 | 0 | 0 | 0 | D̄ = .167 |
| off Pcak | 2 | 0 | o | 0 | S _d = .167 |
| | 3 | 1 | 0 | 1. | t = 1 Accept Ho |
| | 4 | 0 | O | 0 | |
| | 5 | 0 | . О | 0 | |
| | 6 | o [.] . | 0 | 0 | |

table C.19
t-Test analysis of reduction in Stops for southbound Washington Street

| TIME PERIOD | RUN # | STOPS BEFORE (B) | STOPS AFTER (A) | DIFF B-A (D) | REMARKS AND CALCULATIONS |
|----------------|----------|------------------------|-----------------------|--------------------|--------------------------------|
| AM | 1 | 0 | 0 | 0 | D =5 |
| Peak | 2 | 0 | 0 . | 0 | $s_{\overline{d}} = .223$ |
| | 3 | 0 | 1 | -1 | $t = -2.23$ Accept H_0 |
| | 4 | 0 | 0 | o | |
| | 5 | 0 | 1 | -1 | |
| | 6 | 0 | 1 | -1 | |
| Noon | 1 | 1 | 0 | 1 | $\overline{D} = .333$ |
| Peak | 2 | 0 | 0 | 0 | $s_{\overline{d}} = .210$ |
| | 3 | 0 | 0 | 0 | t = 1.58 Accept H _o |
| | 4 | 0 | . 0 | 0 | c = 1.36 Accept no |
| | 5 | . 0 | 0 | 0 | |
| | 6 | 1 | 0 | 1 | |
| • | | _ | Ŭ | _ | |
| PM Peak | 1 | 0 | 0 | 0 | $\bar{D} = .167$ |
| reak | 2 | 0 | 0 | 0 | $s_{\overline{d}} = .167$ |
| | 3 | 1 . | 0 | 1 | t = 1 Accept H _o |
| | 4 | . 0 | .0 | 0 | |
| | 5 | 0 | 0 | О | |
| | 6 | 0 | 0 | 0 | · |
| Off | ! ! , | 0 | 0 | o | $\bar{D} = .167$ |
| Peak | 1 2 | 0 | 0 | 0 | $S_{\overline{d}} = .167$ |
| | 3 | 1 | 0 | . 1 | t = 1 Accept H _o |
| | 4 | 0 | 0. | | - 0 |
| | 5 | 0 | 0 | 0 | |
| | 6 | 0- | 0 | 0 | · |
| | | | | | |

table C.20 table character analysis of reduction in stops for northbound georgia street

| TIME PERIOD | RUN # | STOPS BEFORE (B) | STOPS AFTER (A) | DIFF B-A (D) | REMARKS AND CALCULATIONS |
|----------------|----------|------------------------|-----------------------|--------------------|--------------------------------|
| AM | ı | 3 | 0 | 3 | D = 2.5 |
| Peak | 2 | 3 | 0 . | 3 | $S_{\overline{d}} = .341$ |
| | . 3 | 1 | 0 | 1 | t = 7.32 Accept H _o |
| | 4 | 2 | 0 | 2 | |
| | 5 | 3 | 0 | 3 | |
| | 6 | 3 | 0 | 3 | |
| Noon | 1 | 4 | . 2 | 2 | D = 1.16 |
| Peak | 2 | 2 | 3 | -1 | $S_{\overline{d}} = .477$ |
| | 3 | . 2 | -1 | 1 | t = 2.44 Reject H _o |
| | 4 | 4 | 2 | 2 | |
| | 5 | 4 | 2 | 2 | |
| | 6 | 4 | 3 | 1 | , |
| PM | 1 | 4 | 0 | 4. | D = .5 |
| Peak | 2 | 2 | 3 | -1 | $S_{\overline{d}} = .718$ |
| | 3 | 3 | 3 | 0 | t = .695 Accept H |
| | 4 | 3 | 3 | 0 | |
| | 5 | 3 | 3 | 0 | |
| | 6 | 2 | 2 | 0 | |
| Off | 1 | 2 | 0 | 2 | $\bar{D} = 2.5$ |
| Peak | 2 | 4 | 0 - | 4 | s _ā = .341 |
| | 3 | 3 . | o | 3. | t = 7.32 Reject H |
| | 4 | 2 5 | o | 2 | |
| | 5 | 2 | 0 | 2 . | |
| | 6 | 2 | 0 | 2 | |

TABLE C.21
t-TEST ANALYSIS OF REDUCTION IN STOPS FOR SOUTHBOUND GEORGIA STREET

| TIME PERIOD | RUN # | STOPS BEFORE (B) | STOPS AFTER (A) | DIFF B-A (D) | . REMARKS AND CALCULATIONS |
|----------------|----------|------------------------|-----------------------|--------------------|--------------------------------|
| AM | 1 | 2 | 0 | 2 | D = 1.16 |
| Peak | 2 | 2 | 0 | 2 | $S_{\overline{d}} = .307$ |
| _ | 3 | 2 | 1 | 1 | t = 3.79 Reject H _o |
| | 4 | 1 | 0 | 1 | |
| | 5 | 1 | 1 | 0 | |
| | 6 | 1 | 0 | 1 | |
| Noon | 1 | 2 | 0 | 2 | $\bar{D} = 2.16$ |
| Peak | 2 | 3 | 1 | 2 | $s_{\overline{d}} = .307$ |
| | 3 | · 3 | 0 | 3 | t = 7.05 Reject H _o |
| | 4 | 2 | 0 | 2 | Ů |
| | 5 | 3 | 0 | 3 | |
| | 6 | 1 | 0 | ·1 | |
| PM | 1 | 2 | 0 | 2 | D = 1.5 |
| Peak | 2 | 2 | 1 . | 1 | $S_{\overline{d}} = .428$ |
| | 3 | 3 | 1 | 2 | t = 3.50 Reject H |
| • | 4 | 3 | 0 | 3 | |
| • | 5 | 2 | 2 | 0 | • |
| | · 6 | 2 | 1 | 1 | |
| Off | 1 | 1 | 1 | 0 | $\overline{D} = .833$ |
| Peak | 2 | 1 | 0 | 1 | $S_{\overline{d}} = .167$ |
| | 3 | 2 | 1 | 1. | t = 5 Reject H |
| | 4 | 2 | 1 | 1 | |
| | 5 | 2 | 1 | 1 | |
| | 6 | 2 . | 1 | 1 | |

table c.22 t-test analysis of reduction in stops for northbound western street

| TIME PERIOD | RUN # | STOPS BEFORE (B) | STOPS AFTER (A) | DIFF B-A (D) | REMARKS AND CALCULATIONS |
|----------------|----------|------------------------|-----------------------|--------------------|---------------------------------|
| AM | 1 | 1 | 0 | 1 | D = .833 |
| Peak | 2 | 0 | 0 | 0 | $S_{\overline{d}} = .167$ |
| | 3 | 1 | 0 | 1 | t = 5 Reject H _o |
| | 4 | 1 | 0 | 1 | |
| | 5 | 1 | o | 1 | · |
| | 6 | 1 | 0 | 1 | |
| Noon | 1 | ; | | | |
| Peak | 2 | | <u> </u> | | |
| • | 3 | - | | | |
| | 4 | | | | Noon Peak Data Incomplete |
| ļ | 5 | | | | |
| | 6 | | | | |
| PM | 1 | | 0 | 0 | D =333 |
| Peak | 2 | 0 | 0 | 0 | $S_{\overline{d}} = .210$ |
| <i>;</i> | 3 | 1 | 1 | 0 | t = -1.58 Accept H _o |
| | 4 | . 0 | 1 | -1 | - |
| · | 5 | 1 | 1 | 0 | · |
| | 6 | 0 | 1 | -1 | |
| 0.5.5 | , | 0 | , | • | 5 - 222 |
| Off Peak | 1 | 0 | 1 | -1 | $\overline{D} =333$ |
| | 2 | 1 | 1 | . 0 | $S_{\overline{d}} = .210$ |
| • | 3 4 | 1 . 1 | 1 1. | 0 | t = -1.58 Accept H |
| | 5 | 0 | 1 | -1 | |
| | 6 | í | 1 | 0 | |

TABLE C.23
t-TEST ANALYSIS OF REDUCTION IN STOPS FOR SOUTHBOUND WESTERN STREET

| TIME PERIOD | RUN # | STOPS BEFORE (B) | STOPS AFTER (A) | DIFF B-A (D) | REMARKS AND CALCULATIONS |
|----------------|----------|------------------------|-----------------------|--------------------|--------------------------------|
| AM | 1 | 0 | 0 | 0 | D = .667 |
| Peak | 2 | 1 | 0 | 1 | $S_{\overline{d}} = .210$ |
| | 3 | 1 | 0 | 1 | t = 3.16 Reject Ho |
| | 4 | 1 | 0 | 1 | |
| | 5 | 0 | 0 | 0 | |
| | 6 | 1 | 0 | 1 | |
| Noon Peak | 1 | | | | |
| reak | 2 | | | | |
| • • | 3 | | | · | Noon Peak Data Incomplete |
| · | 4 | | | | Noon reak Data Incomplete |
| - | 5 | | | | · |
| | 6 | | | | |
| PM Peak | 1 | 2 | 1 | 1 | $\overline{D} = 0$ |
| reak | 2 | 0 | 1 | -1 | $S_{\overline{d}} = .516$ |
| | 3 | 2 | 0 | 2 | t = 0 Accept H _o |
| . - | 4 | 0 | 1 | -1 | · |
| ·. | 5 | 1 | 1 | 0 | |
| | . 6 | 0 | 1 | -1 | |
| Off | 1 | 0 | 0 | 0 | D = .167 |
| Peak | 2 | . 1 | 0 - | 1 | S _d = .307 |
| | 3 | 0 . | 0 | 0. | t = .542 Accept H _o |
| | 4 | 0 | 1 | -1 | |
| | 5 | 1 | - 0 | 1. | |
| | 6 | o _. | 0 | 0 | |

t-TEST ANALYSIS OF REDUCTION IN STOPS FOR EASTBOUND 3rd STREET

| TIME PERIOD | RUN # | STOPS BEFORE (B) | STOPS AFTER (A) | DIFF B-A (D) | REMARKS AND CALCULATIONS |
|----------------|----------|------------------------|-----------------------|--------------------|---------------------------------|
| AM | 1 | 2 | 4 | -2 | D̄ = −1 |
| Peak | 2 | 2 | 3 | -1 | $S_{\overline{d}} = .258$ |
| | 3 | 2 | 3 | -1 | t = -3.87 Accept H _o |
| | 4 | 2 | 3 | -1 | |
| | 5 | 1 | 2 | -1 | - |
| | 6 | 1 | 1 | 0 | |
| Noon | 1 | 2 | 2 | 0 | D = 1.5 |
| Peak | 2 | 4 | 3 | 1 | .S _d = .428 |
| | 3 | 4 | 2 | 2 | t = 3.50 Reject H _o |
| | 4 | 3 | 2 | 1 | |
| | 5 | 4 | 2 | 2 | |
| • | 6 | 5 | 2 | 3 | |
| PM | , 1 | 5 | 4 | 1 | $\bar{\mathbf{D}} = 0$ |
| Peak | 2 | 4 | 3 | -1 | s _d = .365 |
| • | 3 | 3 | 4 | -1 | t = 0 Accept H |
| | 4 | 3 | . 3 | 0 | |
| | 5 | 4 | 3 | 1 | |
| | . 6 | 3 | 3 | . 0 | |
| Off | 1 | 0 | 2 | -2 | , |
| Peak | 2 | 2 | 2 | 0 | s _ā = .333 |
| | 3 | 1 | 2 | | t = -2 Accept H _o |
| | 4 | 3 | 3 | 0 | |
| | 5 | 2 | 3 | -1 | |
| | 6 | 3. | 3 | 0 | |

TABLE C.25
t-TEST ANALYSIS OF REDUCTION IN STOPS FOR WESTBOUND 3rd STREET

| TIME PERIOD | RUN ₽ | STOPS BEFORE (B) | STOPS AFTER (A) | DIFF B-A (D) | REMARKS AND CALCULATIONS |
|----------------|----------|------------------------|-----------------------|--------------------|----------------------------------|
| Ам | 1 | 1 | 2 | -1 | D = .167 |
| Peak | 2 | 3 | 3 | 0 | $S_{\overline{d}} = .307$ |
| | 3 | 4 | 3 | 1 | t = .542 Accept H _o |
| | 4 | 3 | 3 | 0 | |
| | 5 | 4 | 3 | 1 | |
| | 6 | 3 | 3 | 0 | |
| Noon | 1 | 3 | 3 | 0 | D =5 |
| Peak | 2 | 3 | 2 | 1 | $S_{\overline{d}} = .428$ |
| | 3 | . 1 | 2 | -1 | t = -1.167 Accept H _o |
| | 4 | 1 | - 2 | -1 | · |
| | 5 | 1 | 3 | - 2 | |
| | 6 | 3 . | 2 | . 0 | |
| PM Peak | 1 | 2 | 3 | -1 | D = 1 |
| 1 Car | 2 | 3 | 3 | 0 | $S_{\overline{d}} = .632$ |
| | 3 | 5 | . 2 | 3 | t = 1.58 Accept H |
| | 4 | . 4 | 2 | 2 | |
| | 5 | '4 | 2 | 2 | • |
| | 6 | 2 | 2 | 0 | |
| Off | 1 | 5 | 4 | 1 | D = 2.5 |
| Peak | 2 | 3 | 1 | 2 | $S_{\overline{d}} = .428$ |
| | 3 | 4 | 1 | · 3 _. | t = 5.84 Reject H _G |
| • | 4 | 3 - | 1 | 2 | |
| | 5 | 5 | 1 | 4 | |
| | 6 | 4 | 1 | 3 | |

TABLE C.26
t-TEST ANALYSIS OF REDUCTION IN STOPS FOR WESTBOUND 6th STREET

| TIME PERIOD | RUN # | STOPS BEFORE (B) | STOPS AFTER (A) | DIFF B-A (D) | REMARKS AND CALCULATIONS |
|----------------|----------|------------------------|-----------------------|--------------------|----------------------------------|
| AM | 1 | 3 | 2 | 1 | D = −.5 |
| Peak | 2 | 3 | 5 | -2 | $S_{\overline{d}} = .763$ |
| | 3 | 3 | 3 | 0 | t = -0.654 Accept H _o |
| | 4 | 2 | 5 | -3 | |
| | 5 | 2 | 3 | -1 | |
| | 6 | 3 | 1 | 2 | · |
| Noon | 1 | 3 | ·. 0 | 3 | |
| Peak | 2 | 4 | 0 | 4 | $S_{\overline{d}} = .258$ |
| | 3 | 3 | ٠0 | 3 | t = 11.62 Reject H _o |
| | 4 | . 2 | o | 2 | |
| • | 5 | 3 | 0 | 3 | |
| | 6 | 3 | 0 | 3 | · |
| PM · | 1 | 3 | 5 | -2 | $\overline{D} = -1.5$ |
| Peak | 2 | 4 | 4 | 0 | $S_{\overline{d}} = .428$ |
| | 3 | 4 | 5 | -1 | t = -3.50 Accept H _o |
| | 4 | 2 | 4 | -2 | • |
| | 5 | 2 | 5 | - 3 | |
| | . 6 | 3 | 4 | -1 | |
| Off | 1 | 5 | 2 | 3 | $\bar{D} = 1.5$ |
| Peak | 2 | 3 | 3 - | 0 | $s_{\overline{d}} = .428$ |
| .• | 3 | 3 | 1 | 2 . | t = 3.50 Reject Ho |
| ٠,٠ | 4 | 3 | 2 | 1 | |
| | 5 | 3 | . 2 | 1. | |
| | 6 | 3 | 1 | 2 | |

t-TEST ANALYSIS OF REDUCTION IN STOPS FOR EASTBOUND 6th STREET

| TIME PERIOD | RUN # | STOPS BEFORE (B) | STOPS AFTER (A) | DIFF B-A (D) | . REMARKS AND CALCULATIONS |
|----------------|----------|------------------------|-----------------------|--------------------|---|
| AM | 1 | 6 | 5 | 1 | D̄ = .333 |
| Peak | . 2 | 4 | 4 | 0 | $S_{\overline{d}} = .494$ |
| | 3 | 5 | 6 | -1 | t = .674 Accept H |
| | 4 | 5 | 4 | 1 | |
| | 5 | 5 | 3 | 2 | |
| | 6 | 5 | 6 | -1 | |
| Noon | 1 | . 5 | 5 | - | $\bar{D} = .5$ |
| Peak | 2 | . 4 | 5 | -1 | $S_{-d} = .428$ |
| | 3 | 5 | 5 | 0 | t = 1.16 Accept H _o |
| ; | 4 | 7 | 5 | 2 | |
| : | 5 | 6 | 5 | 1 | |
| | 6 | 6 | 5 | 1 | · |
| PM Peak | 1 | 4 | 5 | -1 | D =833 |
| 1 Ear | 2 | 4 | 5 . | -1 | $S_{\overline{d}} = .307$ |
| : | 3 | 4 | 5 | -1 | t = -2.71 Accept H |
| | 4 | 5 | 5 | 0 | |
| | 5 | 4 | 6 | -2 | • |
| • | . 6 | 4 | 4 | 0 | : |
| Off Peak | ٠1 | 5 | 5 | 0 | D = .167 |
| reak | 2 | 6 | 6 | 0 | $S_{\overline{d}} = .167$ |
| | 3 | 5 . | 5 | ٥. | t = 1 Accept H |
| | 4 | 6 | 6 | 0 | |
| | 5 | 6 | 6 | 0 | |
| | 6 | 6. | 5 | 1 | |

table c.28

t-test analysis of reduction in stops for Eastbound 7th Street

| TIME PERIOD | RUN ∯ | STOPS BEFORE (B) | STOPS AFTER (A) | DIFF B-A (D) | REMARKS AND CALCULATIONS |
|----------------|----------|------------------------|-----------------------|--------------------|---------------------------------|
| AM Peak | 1 | 4 | 3 | 1 | D ≈ .833 |
| 1 Can | 2 | 5 | 4 | 1 | $S_{\overline{d}} = .542$ |
| | 3 | 5 | 2 | 3 | t ≈ 1.535 Accept H _o |
| | 4 | 4 | 3 | 1 | |
| | 5 | 2 | 3 | -1 | |
| | 6 | 1 | 1 | 0 | |
| Noon Peak | 1 | 6 | 1 | 5 | D = 2.67 |
| reak | 2 | 3 | 2 | 1 | $S_{\bar{d}} = .614$ |
| | 3 | 4 | 2 | 2 | t = 4.34 Reject H _o |
| | 4 | 4 | . 0 | 4 | • |
| | 5 | 4 | 2 | 2 | |
| | 6 | 4 | 2 | 2 | |
| PM | 1 | 4 | 2 | 2 | D = 2.5 |
| Peak | 2 | 5 | 3 | 2 | $S_{\overline{d}} = .5$ |
| | 3 | 5 | 3 | 2 | t = 5 Reject H _o |
| | 4 | . 6 | 4 | 2 | |
| | 5 | 6 | 1 | 5 | • |
| | 6 | 6 | 4 | 2 | |
| Off | 1 | 4 | 1 | 3 | D = 3 |
| Peak | 2 | 3 | 1 | 2 | $s_{\overline{d}} = .577$ |
| | 3 | 3 | 2 | · 1, | t = 5.19 Reject H ₀ |
| | 4 | 4 | 1. | 3 | |
| | 5 | 6 | 1 | 5 | |
| | 6 | 5 | 1 | 4 | |

table C.29
t-TEST ANALYSIS OF REDUCTION IN STOPS FOR WESTBOUND 8th STREET

| TIME PERIOD | RUN # | STOPS BEFORE (B) | STOPS AFTER (A) | DIFF B-A (D) | REMARKS AND CALCULATIONS |
|----------------|----------|------------------------|-----------------------|--------------------|--------------------------------|
| AM | 1 | 5 | 3 | 2 | D = 1.33 |
| Peak | 2 | 5 | 2 | 3 | $S_{\overline{d}} = .667$ |
| | 3 | 4 | 3 | 1 | t = 2 Accept H |
| | 4 | 4 | 1 | 3 | |
| | 5 | 2 | 2 | 0 | |
| | 6 | 3 | 4 | -1 | |
| Noon | 1 | 1 | 1 | 0 | $\vec{D} = 2.17$ |
| Peak | 2 | 5 | 1 | 4 | $s_{\overline{d}} = .600$ |
| | 3 | 3 | ·2 | 1 | t = 3.61 Reject H _o |
| | 4 | 4 | 1 | 3 | |
| | 5 | 4 | 1 | 3 | |
| • | 6 | 3 | 1 | 2 | · |
| PM | 1 | 2 | 1 | 1 | $\bar{D} = 1.67$ |
| Peak | 2 | 4 | 2 | 2 | $S_{\overline{d}} = .421$ |
| | 3 | 4 | 1 | 3 | t = 3.95 Reject H _o |
| | 4 | 4 | . 4 | 0 | Keyece no |
| | 5 | 3 | 1 | 2 | |
| | 6 | 4 | 2 | . 2 | |
| | | · | | _ | |
| Off Peak | 1 | 6 | 1 | 5 | $\bar{D} = 3.33$ |
| | 2 | 5 | 4 - | 1 | $s_{\overline{d}} = .614$ |
| | 3 | 5 . | 2 | 3 . | t = 5.42 Reject H _o |
| | 4 | 6 | 1 | 5 | |
| | 5 | 4 | 1 | 3 . | |
| | 6 | 5. | 2 | 3 | |

table C.30
t-test analysis of reduction in stops for Eastbound 9th street

| TIME PERIOD | RUN # | STOPS BEFORE (B) | STOPS AFTER (A) | DIFF B-A (D) | REMARKS AND CALCULATIONS |
|----------------|----------|------------------------|-----------------------|--------------------|-----------------------------------|
| AM | 1 | 4 | 5 | -1 | D = .833 |
| Peak | 2 | 6 | 4 | 2 | $S_{\overline{d}} = .872$ |
| | 3 | 4 | 5 | , - 1 | t = .955 Accept H |
| | 4 | 4 | 2 | 2 | |
| | 5 | 4 | 5 | -1 | · |
| · | 6 | 6 | 2 · | 4 | |
| Noon | 1 | 4 | 3 | 1 | D = 1.5 |
| Peak | 2 | 5 | 3 | 2 | $S_{\overline{d}} = .428$ |
| • | 3 | 6 | ·3 | 3 | t = 3.50 Reject H _o |
| • | 4 | 4 | 3 | 1 | |
| | 5 | 5 | 3 | 2 | |
| | 6 | 3 | 3 | 0 | • |
| PM Peak | 1 | 4 | 2 | 2 | $\cdot \overline{\mathbf{D}} = 0$ |
| · | . 2 | 3 | 4 | -1 | $S_{\overline{d}} = .683$ |
| | 3 . | . 4 | 5 . | -1 | t = 0 Accept Ho |
| | 4 | 7 | - 5 | -2 | |
| | 5 | 4 . | 2 | . 2 | |
| | 6 | 4 | 4 | 0 | |
| Off | 1 | 4 | 2 | 2 | D = 3.67 |
| Peak | . 2 | 6 | 2 - | 4 | $S_{\overline{d}} = .421$ |
| r.* | 3 | 4 . | 1 | 3 | t = 8.69 Reject H |
| | 4 | 5 | 0 | · 5 | |
| | 5 | . 4 | . 0 | 4 . | |
| | 6 | 4. | 0 | 4 | ٠. |

APPENDIX D

t-TEST EVALUATION OF NUMBER OF STOPS
IN ENTIRE SYSTEM

table d.1

t-Test evaluation of number of stops in entire system*

| Street | H _o : S _A = S _B Direction | H _A : S _A < S _B Period | Stops Before (B) | Stops After (A) | Diff. B - A (D) |
|-------------|---|--|------------------------|-----------------------|----------------------|
| Adams | NB | AM Peak Noon Peak PM Peak | 7 9 10 | 1 5 19 | 6 4 - 9 |
| | SB | AM Peak Noon Peak PM Peak Off Peak | 6 9 9 10 | 0 13 8 12 | 6 -4 1 -2 |
| Amar. Blvd. | EB | AM Peak Noon Peak PM Peak Off Peak | 5 2 5 0 | 0 0 12 0 | 5 2 -7 0 |
| | WB | AM Peak Noon Peak PM Peak Off Peak | 2 1 2 0 | 0 1 1 0 | 2 0 1 0 |
| Buchanan | NB | AM Peak Noon Peak PM Peak Off Peak | 13 7 12 7 | 5 6 2 4 | 8 1 10 3 |
| Filmore | NB | AM Peak Noon Peak PM Peak Off Peak | 7 14 9 7 | 5 1 4 7 | 2 13 5 0 |
| Pierce | SB | AM Peak Noon Peak PM Peak Off Peak | 6 13 19 8 | 6 5 7 9 | 0 8 12 -1 |
| Taylor | SB | AM Peak Noon Peak PM Peak Off Peak | 13 14 16 13 | 3 1 14 10 | 10 13 2 3 |
| Polk | NB | AM Peak Noon Peak PM Peak Off Peak | 17 19 24 22 | 11 32 15 25 | 6 -13 9 -3 |

TABLE D.1 (Continued)

| Street | H _o : S _A = S _B Direction | H _A : S _A < S _B Period | Stops Before (B) | Stops After (A) | Diff. B - A (D) |
|------------|--|--|------------------------|-----------------------|-----------------------|
| Polk | SB | AM Peak Noon Peak PM Peak Off Peak | 25 26 29 25 | 22 22 21 25 | 3 4 8 0 |
| Tyler | NB | AM Peak Noon Peak PM Peak Off Peak | 16 12 12 21 | 12 11 9 7 | 4 1 3 14 |
| Harrison | SB | AM Peak Noon Peak PM Peak Off Peak | 18 14 17 21 | 10 11 7 1 | 8 3 10 20 |
| Van Buren | NB | AM Peak Noon Peak PM Peak Cff Peak | 17 17 15 27 | 1 2 18 23 | 16 15 -3 4 |
| Jackson | SB | AM Peak Noon Peak PM Peak Off Peak | 10 10 2 17 | 26 18 12 13 | -16 -8 -10 4 |
| Washington | NB | AM Peak Noon Peak PM Peak Off Peak | 4 6 11 1 | 5 2 11 0 | -1 4 0 1 |
| | SB | AM Peak Noon Peak PM Peak Off Peak | 0 2 1 1 | 3 0 0 0 | -3 2 1 1 |
| Georgia | NB | AM Peak Noon Peak PM Peak Off Peak | 15 20 17 15 | 0 13 14 0 | 15 7 3 15 |
| | SB | AM Peak Noon Peak PM Peak Off Peak | 9 14 14 10 | 2 1 5 5 | 7 13 9 5 |

TABLE D.1 (Continued)

| Street | H _o : S _A = S _B Direction | H _A : S _A < S _B Period | Stops Before (B) | Stops After (A) | Diff. B - A (D) |
|---------|--|--|------------------------|-----------------------|-----------------------|
| Western | NB | AM Peak PM Peak Off Peak | 5 2 4 | 0 4 6 | 5 -2 -2 |
| | SB | AM Peak PM Peak Off Peak | 4 5 2 | 0 5 1 | 4 0 1 |
| 3rd | ЕВ | AM Peak Noon Peak PM Peak Off Peak | 10 22 22 29 | 16 13 20 15 | -6 9 2 4 |
| | WB | AM Peak Noon Peak PM Peak Off Peak | 18 12 20 18 | 17 14 14 15 | 1 -2 6 3 |
| 6th | EB | AM Peak Noon Peak PM Peak Off Peak | 30 33 25 34 | 28 30 30 33 | 2 3 -5 1 |
| | WB - | AM Peak Noon Peak PM Peak Off Peak | 16 18 18 17 | 19 0 27 11 | -3 18 -9 6 |
| 7th | EB | AM Peak Noon Peak PM Peak Off Peak | 21 25 32 25 | 16 9 17 7 | 5 16 15 18 |
| 8th | WB | AM Peak Noon Peak PM Peak Off Peak | 23 20 21 25 | 15 7 11 11 | 8 13 10 14 |
| 9th | EB | AM Peak Noon Peak PM Peak Off Peak | 28 27 26 24 | 23 18 22 5 | 5 9 4 19 |
| 10th | EB | AM Peak Noon Peak PM Peak Off Peak | 35 36 24 34 | 35 29 20 43 | 0 7 4 –9 |

TABLE D.1 (Continued)

| Street | H _o : S _A = S _B Direction | H _A : S _A < S _B Period | Stops Before (B) | Stops After (A) | Diff. B - A (D) |
|--------|---|--|------------------------|-----------------------|-----------------------|
| 10th | WB | AM Peak Noon Peak PM Peak Off Peak | 34 20 26 19 | 25 6 24 5 | 9 14 2 14 |
| 11th | EB | AM Peak Noon Peak PM Peak Off Peak | 18 7 13 13 | 23 15 26 19 | -5 -8 -13 -6 |

^{*}The data in this table were used in the calculation of the t-test.

For One-tail test:
$$t_{.05} = 1.66$$
 (d.f. = 115)
 $t_{calc.} = 5.47 > 1.66$, * Reject H_o, Accept H_A

APPENDIX E

CHI SQUARE EVALUATION OF NUMBER OF STOPS

TABLE E.1
CHI SQUARE EVALUATION OF NUMBER OF STOPS

| STREET | DIRECTION | PERIOD | AFTER (OBSERVED) | BEFORE (EXPECTED) | $\frac{(A-B)^2}{B}$ |
|-------------|-----------|---|----------------------|----------------------|-------------------------------|
| Adams | NB | AM Peak Noon Peak PM Peak | 1 5 19 | 7 9 10 | 5.14 1.78 8.1 |
| | SB | AM Peak Noon Peak PM Peak Off Peak | 0 13 8 12 | 6 9 9 10 | 6.0 1.78 0.11 0.4 |
| Amar. Blvd. | ЕВ | AM Peak Noon Peak PM Peak Off Peak | 0 0 12 0 | 5 2 5 0 | 5.0 2.0 9.8 0 |
| | WB | AM Peak Noon Peak PM Peak Off Peak | 0 1 1 0 | 2 1 2 0 | 2.0 0 0.5 0 |
| Buchanan | NB | AM Peak Noon Peak PM Peak Off Peak | 5 6 2 4 | 13 7 12 7 | 4.92 0.14 8.33 1.29 |
| Filmore | NB | AM Peak Noon Peak PM Peak Off Peak | 5 1 4 7 | 7 14 9 7 | 0.57 12.07 2.78 0 |
| Pierce | SB | AM Peak Noon Peak PM Peak Off Peak | 6 5 7 9 | 6 13 19 8 | 0 4.92 7.58 0.13 |
| Taylor | SB | AM Peak Noon Peak PM Peak Off Peak | 3 1 14 10 | 13 14 16 13 | 7.69 12.07 0.25 0.69 |
| Polk | NB | AM Peak Noon Peak PM Peak Off Peak | 11 32 15 25 | 17 19 24 22 | 2.12 8.89 3.38 0.41 |

TABLE E.1 (Continued)

| | , | | | | |
|-------------|--------------|---|----------------------|----------------------|-------------------------------|
| STREET | DIRECTION | PERIOD | AFTER (OBSERVED) | BEFORE (EXPECTED) | $\frac{x^2}{(A-B)^2}$ |
| | SB | AM Peak Noon Peak PM Peak Off Peak | 22 22 21 25 | 25 26 29 25 | 0.36 0.62 2.21 0.0 |
| Tyler | NB | AM Peak Noon Peak PM Peak Off Peak | 12 11 9 7 | 16 12 12 21 | 1.0 0.08 0.75 9.33 |
| Harrison | SB | AM Peak Noon Peak PM Peak Off Peak | 10 11 7 1 | 18 14 17 21 | 3.56 0.64 5.88 19.05 |
| Van Buren | NB | AM Peak Noon Peak PM Peak Off Peak | 1 2 18 23 | 17 17 15 27 | 15.06 13.24 0.6 0.59 |
| Jackson | SB | AM Peak Noon Peak PM Peak Off Peak | 26 18 12 13 | 10 10 2 17 | 25.6 6.4 50.0 0.94 |
| Washington | NB | AM Peak Noon Peak PM Peak Off Peak | 5 2 11 0 | 4 6 11 1 | 0.25 2.67 0.0 1.0 |
| | SB | AM Peak Noon Peak PM Peak Off Peak | 3 0 0 0 | 0 2 1 1 | 2.0 1.0 1.0 |
| Georgia | NB | AM Peak Noon Peak PM Peak Off Peak | 0 13 14 0 | 15 20 17 15 | 15.0 2.45 0.53 15.0 |
| | SB | AM Peak Noon Peak PM Peak Off Peak | 2 1 5 5 | 9 14 14 10 | 5.44 12.07 5.79 2.50 |

TABLE E.1 (Continued)

| STREET | DIRECTION | PERIOD | AFTER (OBSERVED) | BEFORE (EXPECTED) | $\frac{X^2}{(A - B)^2}$ |
|---------|-----------|---|----------------------|----------------------|--------------------------------|
| Western | NB | AM Peak PM Peak Off PEak | 0 4 6 | 5 2 4 | 5.0 2.0 1.0 |
| , | SB | AM Peak PM Peak Off Peak | 0 5 1 | 4 5 2 | 4.0 0.0 0.5 |
| 3rd | EB | AM Peak Noon Peak PM Peak Off Peak | 16 13 20 15 | 10 22 22 19 | 3.6 3.68 0.18 0.84 |
| | WB | AM Peak Noon Peak PM Peak Off Peak | 17 14 14 15 | 18 12 20 18 | 0.06 0.33 1.80 0.50 |
| 6th | EB | AM Peak Noon Peak PM Peak Off Peak | 28 30 30 33 | 30 33 25 34 | 0.13 0.27 1.0 0.03 |
| | WB | AM Peak Noon Peak PM Peak Off Peak | 19 0 27 11 | 16 18 18 17 | 0.56 18.0 4.5 2.12 |
| 7th | EB | AM Peak Noon Peak PM Peak Off Peak | 16 9 17 7 | 21 25 32 25 | 1.19 10.24 7.03 12.96 |
| 8th | WB | AM Peak Noon Peak PM Peak Off Peak | 15 7 11 11 | 23 20 21 25 | 2.78 8.45 4.76 7.84 |
| 9th | EB | AM Peak Noon Peak PM Peak Off Peak | 23 18 22 5 | 28 27 26 24 | 0.89 3.0 0.62 15.04 |
| 10th | EB | Noon Peak PM Peak Off Peak | 29 20 43 | 36 24 34 | 1.36 0.67 2.38 |

TABLE E.1 (Continued)

| STREET | DIRECTION | PERIOD | AFTER (OBSERVED) | BEFORE (EXPECTED) | $\frac{x^2}{(A-B)^2}$ |
|--------|-----------|---|----------------------|----------------------|------------------------------|
| 10th | WB | AM Peak Noon Peak PM Peak Off Peak | 25 6 24 5 | 34 20 26 19 | 2.38 9.8 0.15 10.32 |
| llth | ЕВ | AM Peak Noon Peak PM Peak Off Peak | 23 15 26 19 | 18 7 13 13 | 1.39 9.14 13.0 2.77 |

n = 116

 $\Sigma = 520.73$

APPENDIX F COMPUTATION OF DELAY PER DAY

TABLE F.1

COMPUTATION OF DELAY PER DAY IN BEFORE AND AFTER PERIODS

| | | | | ; — | | | | BE | BEFCRE | | | | | | | AFTER | 8 | | | |
|----------------|------------|--------------|------------|-------------|------------|--------------|---------------|--------------|------------|--------------|------------|-------------|------------|------------------|------------|-------------|------------|--------------|------------|-------------|
| STREET | | VOLUME | UME | | | DELAY | Y LE (SEC) | (5) | | DELAY (1 | (VEH-HR) | | - | DELAY VEHICLE | (SEC) | | | DELAY (1 | (Vен-нк) | |
| | AM Peak | Noon Peak | PM Peak | 0ff Peak | AM Peak | Noon Peak | PN Peak | Of f Peak | AM Peak | Noon Peak | PM Peak | Off Peak | AM Peak | Noon Peak | PN Peak | Off Peak | AM Peak | Noon Peak | PM Peak | Off Peak |
| Adams NB | 1200 | 700 | 650 | 5900 | 4.85 | 14.5 | 36.2 | 1 | 1.6 | 2.8 | 6.5 | 1 | 3.5 | 13.3 | 62.5 | 1 | 1.2 | 2.6 | 11.3 | 1 |
| Adams SB | 200 | 200 | 950 | 3700 | 10.5 | 14.5 | 25.5 | 21.3 | 0.6 | 2.0 | 6.7 | 21.9 | 0.0 | 41,7 | 18.5 | 36.5 | 0 | 5.8 | 6.4 | 37.5 |
| Amar. Blvd. EB | 650 | 750 | 1100 | 8100 | 2.3 | 0.8 | 12.3 | 0.0 | 0.4 | 0.2 | 3.8 | 0 | 0.0 | 0.0 | 14.5 | 0.0 | 0 | 0 | 4.5 | 0 |
| Amar. Blvd. WB | 550 | .550 | 750 | 4900 | 0.5 | 0.5 | 1,2 | 0.0 | 0.1 | 0.1 | 0,3 | 0 | 0.0 | 0,3 | 0.3 | 0.0 | 0 | 0 | 0.1 | 0 |
| Buchanan NB | 1700 | 1100 | 1800 | 6400 | 43.8 | 24.2 | 42.0 | 19.3 | 20.7 | 7.4 | 21.0 | 34.3 | 23.8 | 23.2 | 1.3 | 23.5 | 11.2 | 7.1 | 0.7 | . 41.8 |
| Fillmore NB | 1050 | 950 | 950 | 9750 | 30.2 | 35.0 | 25.7 | 37.0 | 8.8 | 9.5 | 6.8 | 100.2 | 16.0 | 5.7 | 3.5 | 20.3 | 4.7 | 1.5 | 0.9 | 55.2 |
| Pierce SB | 009 | 950 | 1600 | 8850 | 19.0 | 36.8 | 54,5 | 11.5 | 3.2 | 9.7 | 24.2 | 28.3 | 8.7 | 0.5 | 0.9 | 22.8 | 1,5 | 2.5 | 2.7 | 56.1 |
| Taylor SB | 650 | 950 | 1600 | 8450 | 33.0 | 43.3 | 80.7 | 22.3 | 0.9 | 11.4 | 35.9 | 52.3 | 14.5 | 4.7 | 31.2 | 16.5 | 2.6 | 1.2 | 13.9 | 38.7 |
| Polk NB | 150 | 300 | 400 | 1150 | 38.2 | 49.5 | 53.7 | 78.8 | 1.6 | 4.1 | 9.0 | 25.2 | 25.2 | 84,8 | 59.2 | 40.0 | 1.1 | 7.1 | 9.9 | 12.8 |
| Polk'SB | 150 | 300 | 400 | 1150 | 49.7 | 83,3 | 73.8 | 56.8 | 2.5 | 6.9 | 8.2 | 18.1 | 67.7 | 46.8 | 71.0 | 56.7 | 2.8 | 3.9 | 7.9 | 18.1 |
| Tyler NB | 150 | 250 | 200 | 3100 | 7.2 | 12.5 | 8,3 | 10.7 | 0.3 | 0.9 | 0.5 | 9.5 | 24.5 | 36.7 | 18,2 | 17.8 | 1.0 | 2.5 | 1.0 | 15.3 |
| Harrison SB | 300 | 200 | 1100 | 3000 | 26.3 | 20.0 | 39.0 | 29.0 | 2.2 | 2.8 | 11.9 | 24.2 | 6.2 | 40.3 | 11.8 | 0.3 | 0.5 | 5.6 | 3.6 | 0.3 |
| Van Buren NB | 200 | 100 | 100 | 1000 | 19.3 | 15.0 | 24.7 | 16.0 | 1.1 | 0.4 | 0.7 | 4.4 | 0.7 | 8.2 | 31.3 | 7.7 | 0 | 0.2 | 0.9 | 2.1 |
| Jackson SB | 100 | 350 | 650 | 2600 | 23.8 | 17.7 | 1.7 | 10.8 | 0.7 | 1.7 | 0.3 | 7.8 | 74.7 | 14.5 | 30.5 | 4.2 | 2.1 | 1.4 | 5.5 | 3.0 |
| 3rd EB | 350 | 400 | 450 | 2900 | 26.7 | 34.0 | 41.2 | 42.5 | 2.6 | 3.8 | 5.2 | 34.2 | 63.3 | 15,8 | 110.8 | 38.5 | 6.2 | 1.8 | 13.9 | 31.0 |
| 3rd WB | 350 | 400 | 200 | 3000 | 44.8 | 25.8 | 47.3 | 47.2 | 4.4 | 2.9 | 9.9 | 39.3 | 88.8 | 12.8 | 7.07 | 23.0 | 8.6 | 1.4 | 9.8 | 19.2 |

TABLE F.1 (Continued)

| | | | | | | | | BE | FORE | • | | | | | | ٨F٦ | ER | | | |
|---------------|------------|--------------|------------|-------------|------------|--------------|------------|-------------|------------|--------------|------------|-------------|------------|-----------------|------------|-------------|------------|--------------|------------|-------------|
| STREET | | VOL | JUME | | | DELA | CLE (SE | C) | ŗ | DAY (| VEH-HF | ι) | | DELAY VEHICI | | c) | Ξ | DAY (| VEH-HF | 1) |
| | AM Peak | Noon Peak | PH Peak | Off Peak | AM Peak | Noon Peak | PM Peak | Off Peak | AM Peak | Noon Peak | PM Peak | Off Peak | AM Peak | Noon Peak | PM Peak | Off Peak | AM Peak | Noon Peak | PM Peak | Off Peak |
| 6th EB | 200 | 150 | 300 | 1150 | 99.8 | 93.7 | 82.5 | 140.0 | 5.5 | 3.9 | 6.9 | 44.7 | 100.7 | 109.0 | 105.3 | 106.0 | 5.6 | 4.5 | 8.8 | 33.9 |
| 6th WB | 300 | 600 | 500 | 4400 | 57.7 | 54.5 | 66.8 | 74.2 | 4.8 | 9.9 | 9.3 | 101.0 | 54.2 | 0.0 | 96.2 | 47.3 | 4.5 | 0 | 13.4 | 64.4 |
| 7th EB | 400 | 500 | 650 | 3550 | 36.5 | 54.8 | 94.3 | 34.0 | 4.1 | 7.6 | 17.0 | 33.5 | 40.3 | 7.3 | 93.5 | 28.5 | 4.5 | 1.0 | 16.9 | 28.1 |
| 8th WB | 750 | 450 | 650 | 3550 | 86.5 | 64.7 | 73.5 | 78.8 | 18.0 | 8.1 | 13.3 | 77.7 | 69.8 | 13.7 | 37.7 | 16.2 | 14.5 | 1.7 | 6.8 | 16.C |
| 9th EB | 150 | 150 | 200 | 1500 | 36.7 | 56.5 | 44.5 | 91.7 | 1.5 | 2.4 | 2.5 | 38.2 | 57.5 | 100.3 | 109.5 | 8.8 | 2.4 | 4.2 | 6.1 | 3.7 |
| 10th EB | 200 | 250 | 350 | 2200 | 123.8 | 119.3 | 101.8 | 167.8 | 6.9 | 8,3 | 9.9 | 102.5 | 106.5 | 79.2 | 77.2 | 124.0 | 5.9 | 5.5 | 7.5 | 75.8 |
| 10th WB | 500 | 750 | 1050 | 6050 | 90.2 | 47.3 | 117.5 | 60.0 | 13.8 | 9.9 | 34.3 | 100.8 | 89.0 | 10.2 | 100.2 | 18.3 | 13.6 | 2.1 | 29.2 | 30.8 |
| 11th EB | 200 | 250 | 400 | 1900 | 90.3 | 13.0 | 39.2 | 17.5 | 5.0 | 0.9 | 4.4 | 9.2 | 114.8 | 22.3 | 120.8 | 38.3 | 6.4 | 1.5 | 13.4 | 20.2 |
| Washington NB | 650 | 500 | 650 | 4900 | 3.5 | 2.5 | 30.2 | 5.7 | 0.6 | 0.3 | 5.5 | 7.8 | 4.3 | 0.8 | 48.3 | 0.0 | 0.8 | 0.1 | 8.7 | 0 |
| Washington SB | 1350 | 900 | 950 | 8450 | 0.0 | 8.3 | 1.5 | 3.2 | 0 | 0.4 | 0.4 | 7.5 | 4.3 | 0.0 | 0.0 | 0.0 | 1.6 | 0 | 0 | 0 |
| Georgia NB | 500 | 700 | 1000 | 6600 | 42.3 | 89.0 | 93.8 | 27.0 | 6.5 | 17.3 | 26.1 | 49.5 | .0.0 | 56.7 | 20.5 | 0.0 | 0 | 11.0 | 5.7 | 0 |
| Georgia SB | 260 | 800 | 1200 | 6700 | 29.3 | 47.3 | 84.7 | 32.2 | 2.1 | 10.5 | 28.2 | 59.9 | 1.5 | 11.8 | 6.0 | 5.3 | 0.1 | 2.6 | 2.0 | 9.5 |
| Western NB | 500 | 600 | 750 | 5550 | 18.0 | | 12.7 | 23.5 | 2.8 | - | 2.6 | 36.2 | 0.0 | - | 3.7 | 7.7 | 0 | - | 0.8 | 11.9 |
| Western SB | 500 | 750 | 1100 | 8150 | 7.3 | - | 18.3 | 6.0 | 1.1 | - | 3.8 | 13.6 | 0.0 | - | 6.5 | 1.0 | 0 | - | 1.4 | 2.3 |

TABLE F.2

COMPILATION OF DELAY PER DAY BY SECTION AND FOR TOTAL SYSTEM IN BEFORE AND AFTER PERIODS*

| | | BE | FORE | | | | AI | TER | | |
|----------------|------------|--------------|-------------|--------------|--------|------------|--------------|-------------|--|-------|
| STREET | | | ELAY DAY | | | | | ELAY DAY | | |
| | AM Peak | Noon Peak | PM Peak | Off Peak | Total | AM Peak | Noon Peak | PM Peak | Off Peak | Total |
| Sections 1 & 2 | | | | | | | | | ~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~ | |
| Buchanan | 20.7 | 7.4 | 21.0 | 34.3 | | 11.2 | 7.1 | 0.7 | 41.8 | |
| Fillmore | 8.8 | 9.2 | 6.8 | 100.2 | | 4.7 | 1.5 | 0.9 | 55.2 | |
| Pierce | 3.2 | 9.7 | 24.2 | 28.3 | | 1.5 | 2.5 | 2.7 | 56.1 | |
| Taylor | 6.0 | 11.4 | 35.9 | 52.3 | | 2.6 | 1.2 | 13.9 | 38.7 | |
| Polk NB | 1.6 | 4.1 | 6.0 | 25.2 | | 1.1 | 7.1 | 6.6 | 12.8 | |
| Polk SB | 2.5 | 6.9 | 8.2 | 18.1 | | 2.8 | 3.9 | 7.9 | 18.1 | |
| Tyler | 0.3 | 0.9 | 0.5 | 9.2 | | 1.0 | 2.5 | 1.0 | 15.3 | |
| Harrison | 2.2 | 2.8 | 11.9 | 24.2 | | 0.5 | 5.6 | 3.6 | 0.3 | |
| Van Buren | 1.1 | 0.4 | 0.7 | 4.4 | | 0 | 0.2 | 0.9 | 2.1 | |
| Jackson | 0.7 | 1.7 | 0.3 | 7.8 | | 2.1 | 1.4 | 5.5 | 3.0 | |
| 3rd EB | 2.6 | 3.8 | 5.2 | 34.2 | | 6.2 | 1.8 | 13.9 | 31.0 | |
| 3rd WB | 4.4 | 2.9 | 6.6 | 39.3 | | 8.6 | 1.4 | 9.8 | 19.2 | |
| 6th EB | 5.5 | 3.9 | 6.9 | 44.7 | | 5.6 | 4.5 | 8.8 | 33.9 | |
| 6th WB | 4.8 | 9.9 | 9.3 | 101.0 | | 4.5 | 0 | 13.4 | 64.4 | |
| 7th | 4.1 | 7.6 | 17.0 | 33.5 | | 4.5 | 1.0 | 16.4 | 28.1 | |
| 8th | 18.0 | 8.1 | 13.3 | 77.7 | | 14.5 | 1.7 | 6.8 | 16.0 | |
| 9th | 1.5 | 2.4 | 2.5 | 38.2 | | 2.4 | 4.2 | 6.1 | 3.7 | |
| 10th EB | 6.9 | 8.3 | 9.9 | 102.5 | | 5.9 | 5.5 | 7.5 | 75.8 | |
| 10th WB | 13.8 | 9.9 | 34.3 | 100.8 | | 13.6 | 2.1 | 29.2 | 30.8 | |
| 11th EB | 5.0 | 0.9 | 4.4 | 9.2 | | 6.4 | 1.5 | 13.4 | 20.2 | |
| | 113.7 | 112.2 | 224,9 | 885.1 | 1335.9 | 99.7 | 56.7 | 169.5 | 566.5 | 892, |

TABLE F.2 (Continued)

| _ | | BE | FORE | | | | AF | TER | | |
|----------------------------------|------------|--------------|-------------|-------------|-------|---|--------------|------------|-------------|-------|
| STREET | | | ELAY DAY | | | | | LAY AY | | |
| | AM Peak | Noon Peak | PM Peak | Off Peak | Total | AM Peak | Noon Peak | PM Peak | Off Peak | Total |
| Section 3 | | | | | | | | | | |
| Amar. Blvd. EB Amar. Blvd. WB | 0.4 0.1 | 0.2 0.1 | 3.8 0.3 | 0 0 | | 0 | 0 0 | 4.4 0.1 | 0 0 | |
| | 0.5 | 0.3 | 4.1 | 0 | 4.9 | 0 | 0 | 4.5 | 0 | 4.5 |
| Section 4 | | | | | | | | | | |
| Adams NB | 1.6 | 2.8 | 6.5 | | | 1.2 | 2.6 | 11.3 | _ | |
| Adams SB | 0.6 0.6 | 2.0 | 6.7 5.5 | 21.9 | | 0 | 5.8 | 4.9 8.7 | 37.5 | |
| Washington NB Washington SB | 0.0 | 0.3 | 0.4 | 7.8 7.5 | | $\begin{array}{c} 0.8 \\ 1.6 \end{array}$ | 0.1 0 | 0 | 0 0 | |
| | 2.8 | 5.5 | 19.1 | 37.2 | 64.6 | 3.6 | 8.5 | 24.9 | 37.5 | 74.5 |
| Section 5 | | | | | | | | | | |
| Georgia NB | | 17.3 | 26.1 | 49.5 | | 0 | 11.0 | 5.7 | 0 | |
| Georgia SB | 2.1 | 10.5 | 28.2 | 59.9 | | 0.1 | 2.6 | 2.0 | 9.9 | |
| | 8.6 | 27.8 | 54.3 | 109.4 | 200.1 | 0.1 | 13.6 | 7.7 | 9.9 | 31.3 |

TABLE F.2 (Continued)

| | | BE | FORE | | | | AF | TER | | |
|---------------------------------------|------------|----------------|-------------|--------------|--------|------------|--------------|------------|-------------|-------|
| STREET | | <u>D1</u> I | ELAY DAY | | | | <u>DE</u> | LAY AY | | |
| | AM Peak | Noon Peak | PM Peak | Off Peak | Tota1 | AM Peak | Noon Peak | PM Peak | Off Peak | Total |
| Section 7 Western NB Western SB | 2.8 1.1 | | | 36.2 13.6 | | 0 | | 0.8 1.4 | 11.9 2.3 | |
| | 3.9 | _ | 6.4 | 49.8 | 1664.8 | 0 | - | 2.2 | 14.2 | 1019. |

*TOTAL SYSTEM DELAY - BEFORE - 1664.8

AFTER - 1019.1

TOTAL SYSTEM REDUCTION IN DELAY = $\frac{1664.8 - 1019.1}{1664.8}$ = 38.8%

APPENDIX G t-TEST EVALUATION OF DELAY IN ENTIRE SECTION

TABLE G.1
t-TEST EVALUATION OF DELAY IN ENTIRE SYSTEM*

 $H_o: D_A = D_B$

 $H_A: D_A < D_B$

| $H_0: D_A = D_B$ | | HA: DA C DB | | | |
|------------------|-----------|---|--------------------------|--------------------------|------------------------------------|
| STREET | DIRECTION | PERIOD | DELAY BEFORE (B) | DELAY AFTER (A) | DIFFERENCE B - A (D) |
| Adams | NB | AM Peak Noon Peak PM Peak | 29 87 217 | 21 80 375 | 8 7 - 158 |
| | SB | AM Peak Noon Peak PM Peak Off Peak | 63 87 153 128 | 0 250 111 219 | 63 -163 42 -91 |
| Amar. Blvd. | EB | AM Peak Noon Peak PM Peak Off Peak | 14 5 74 0 | 0 0 87 0 | 14 5 -13 0 |
| | WB | AM Peak Noon Peak PM Peak Off Peak | 3 3 7 0 | 0 2 2 0 | 3 1 5 0 |
| Buchanan | NB | AM Peak Noon Peak PM Peak Off Peak | 263 145 252 116 | 143 139 8 141 | 120 6 244 - 25 |
| Fillmore | NB | AM Peak Noon Peak PM Peak Off Peak | 181 210 154 222 | 96 34 21 122 | 85 176 133 100 |
| Pierce | SB | AM Peak Noon Peak PM Peak Off Peak | 114 221 327 69 | 52 57 36 137 | 62 164 291 -68 |
| Taylor | SB | AM Peak Noon Peak PM Peak Off Peak | 198 260 484 134 | 87 28 187 99 | 111 232 297 35 |
| Polk | NB | AM Peak Noon Peak PM Peak Off Peak | 229 297 322 473 | 151 509 355 240 | 78 -212 -33 233 |

TABLE G.1 (Continued)

| STREET | DIRECTION | PERIOD | DELAY BEFORE (B) | DELAY AFTER (A) | DIFFERENCE B - A (D) |
|-----------|-----------|---|--------------------------|--------------------------|----------------------------|
| Polk | SB | AM Peak Noon Peak PM Peak Off Peak | 358 500 443 341 | 406 281 426 340 | -48 219 17 1 |
| Tyler | NB | AM Peak Noon Peak PM Peak Off Peak | 43 75 50 64 | 147 220 109 107 | -104 -145 -59 -43 |
| Harrison | SB | AM Peak Noon Peak PM Peak Off Peak | 158 120 234 174 | 37 242 71 2 | 121 -122 163 172 |
| Van Buren | NB | AM Peak Noon Peak PM Peak Off Peak | 116 90 148 96 | 4 49 188 46 | 112 41 -40 50 |
| 3rd | ЕВ | AM Peak Noon Peak PM Peak Off Peak | 160 204 247 255 | 380 95 665 231 | -220 109 -418 24 |
| i. | WB | AM Peak Noon Peak PM Peak Off Peak | 269 155 284 283 | 533 77 424 138 | -264 78 -140 145 |
| 6th | ЕВ | AM Peak Noon Peak PM Peak Off Peak | 599 562 495 840 | 604 654 632 636 | -5 -92 -137 204 |
| | WB | AM Peak Noon Peak PM Peak Off Peak | 346 357 401 445 | 325 0 577 284 | 21 357 -176 161 |
| 7th | ЕВ | AM Peak Noon Peak PM Peak Off Peak | 219 329 566 204 | 242 44 561 171 | -23 285 5 33 |

TABLE G.1 (Continued)

| STREET | DIRECTION | PERIOD | DELAY BEFORE (B) | DELAY AFTER (A) | DIFFERENCE B - A (D) |
|------------|-----------|---|---------------------------|--------------------------|-----------------------------|
| 8th | WB | AM Peak Noon Peak PM Peak Off Peak | 519 388 441 473 | 419 82 226 97 | 100 306 215 376 |
| 9th | ЕВ | AM Peak Noon Peak PM Peak Off Peak | 220 339 267 550 | 345 602 657 53 | -125 -263 -390 497 |
| 10th | ЕВ | AM Peak Noon Peak PM Peak Off Peak | 743 716 611 1007 | 639 475 463 744 | 104 241 148 263 |
| | WВ | AM Peak Noon Peak PM Peak Off Peak | 541 284 705 360 | 534 61 601 110 | 7 223 104 250 |
| llth | ЕВ | AM Peak Noon Peak PM Peak Off Peak | 542 78 235 105 | 689 134 725 230 | -147 -56 -490 -125 |
| Washington | NB | AM Peak Noon Peak PM Peak | 21 15 181 | 26 5 290 | -5 10 -109 |
| | SB | AM Peak Noon Peak PM Peak Off Peak | 0 50 9 19 | 26 0 0 0 | -26 50 9 19 |
| Georgia | NB | AM Peak Noon Peak PM Peak Off Peak | 254 534 563 162 | 0 340 123 0 | 254 194 440 162 |
| | SB | AM Peak Noon Peak PM Peak Off Peak | 176 284 508 193 | 9 71 36 32 | 167 213 472 161 |

TABLE G.1 (Continued)

| STREET | DIRECTION | PERIOD | DELAY BEFORE (B) | DELAY AFTER (A) | DIFFERENCE B - A (D) |
|---------|-----------|--------------------------------|------------------------|-----------------------|----------------------------|
| Western | NB | AM Peak PM Peak Off Peak | 108 76 141 | 0 22 46 | 108 54 95 |
| | SB | AM Peak PM Peak Off Peak | 44 110 36 | 0 39 6 | 44 71 30 |

The data in this table were used in the calculation of n = 117 the t-test. B = 45.30 $S_{\overline{d}} = 15.79$ t_{CALC} (2.87) > $t_{.01}$ (2.33)

Reject Ho

 $t_{.05} = 1.66$ Accept HA

 $t_{.01} = 2.33$

t = 2.87

APPENDIX H

t-TEST EVALUATION OF NUMBER OS STOPS BY SECTION

table H.1 ${\tt t-TEST} \ \, {\tt EVALUATION} \ \, {\tt CF} \ \, {\tt NUMBER} \ \, {\tt OF} \ \, {\tt STOPS} \ \, {\tt IN} \ \, {\tt SECTIONS} \ \, 1 \ \, {\tt AND} \ \, 2 \ \, {\tt CALCULATIONS}^{\textstyle \star}$ SECTION 1 AND 2

| STREET | DIRECTION | PERIOD | STOPS BEFORE (B) | STOPS AFTER (A) | DIFFERENCE B - A (D) |
|-----------|-----------|---|------------------------|-----------------------|----------------------------|
| Buchanan | NB | AM Peak Noon Peak PM Peak Off Peak | 13 7 12 7 | 5 6 2 4 | 8 1 10 3 |
| Fillmore | NB | AM Peak Noon Peak PM Peak Off Peak | 7 14 9 7 | 5 1 4 7 | 2 13 5 0 |
| Pierce | SB | AM Peak Noon Peak PM Peak Off Peak | 6 13 19 8 | 6 5 7 9 | 0 8 12 -1 |
| Taylor | SB | AM Peak Noon Peak PM Peak Off Peak | 13 14 16 13 | 3 1 14 10 | 10 13 2 3 |
| Polk | NB | AM Peak Noon Peak PM Peak Off Peak | 17 19 24 22 | 11 32 15 25 | 6 -13 9 -3 |
| | SB | AM Peak Noon Peak PM Peak Off Peak | 25 26 29 25 | 22 22 21 25 | 3 4 8 0 |
| Tyler | NB | AM Peak Noon Peak PM Peak Off Peak | 16 12 12 21 | 12 11 9 7 | 4 1 3 14 |
| Harríson | SB | AM Peak Noon Peak PM Peak Off Peak | 18 14 17 21 | 10 11 7 1 | 8 3 10 20 |
| Van Buren | NB | AM Feak Noon Peak PM Peak Off Peak | 17 17 15 27 | 1 2 18 23 | 16 15 -3 4 |

TABLE H.1 (Continued)

| STREET | DIRECTION | PERIOD | STOPS BEFORE (B) | STOPS AFTER (A) | DIFFERENCE B - A (D) |
|---------|-----------|---|------------------------|-----------------------|----------------------------|
| Jackson | SB | AM Peak Noon Peak PM Peak Off Peak | 10 10 2 17 | 26 18 12 13 | -16 -8 -10 4 |
| 3rd | ЕВ | AM Peak Noon Peak PM Peak Off Peak | 10 22 22 19 | 16 13 20 15 | -6 9 2 4 |
| | WB | AM Peak Noon Peak PM Peak Off Peak | 18 12 20 18 | 17 14 14 15 | 1 -2 6 3 |
| 6th | ЕВ | AM Peak Noon Peak PM Peak Off Peak | 30 33 25 34 | 28 30 30 33 | 2 3 -5 1 |
| | WB | AM Peak Noon Peak PM Peak Off Peak | 16 18 18 17 | 19 0 27 11 | -3 18 -9 6 |
| 7th | ЕВ | AM Peak Noon Peak PM Peak Off Peak | 21 25 32 25 | 16 9 17 7 | 5 16 15 18 |
| 8th | WB | AM Peak Noon Peak PM Peak Off Peak | 23 20 21 25 | 15 7 11 11 | 8 13 10 14 |
| 9th | ЕВ | AM Peak Noon Peak PM Peak Off Peak | 28 27 26 24 | 23 18 22 5 | 5 9 4 19 |
| 10th | ЕВ | AM Peak Noon Peak PM Peak Off Peak | 35 36 24 34 | 35 29 20 43 | 0 7 4 - 9 |

TABLE H.1 (Continued)

| STREET | DIRECTION | PERIOD | STOPS BEFORE (B) | STOPS AFTER (A) | DIFFERENCE B - A (D) |
|--------|-----------|---|------------------------|-----------------------|----------------------------|
| 10th | WB | AM Peak Noon Peak PM Peak Off Peak | 34 20 26 19 | 25 6 24 5 | 9 14 2 14 |
| llth | ЕВ | AM Peak Noon Peak PM Peak Off Peak | 18 7 13 13 | 23 15 26 19 | -5 -8 -13 -6 |

 $[\]overset{\star}{}$ The data in this table were used in the calculation of the t-test.

$$n = 80$$
 $S_{\overline{d}} = 0.885$ $\overline{D} = 4.275$ $t = 4.83 > 1.67$ $t_{.05}(79d.f.) = 1.67$ Reject H_0

TABLE H.2 t-test evaluation of number of stops in sections*

| STREET | DIRECTION | PERIOD | STOPS BEFORE (B) | STOPS AFTER (A) | DIFFERENCE B - A (D) |
|-------------|-----------|---|------------------------|-----------------------|----------------------------|
| Amar. Blvd. | ЕВ | AM Peak Noon Peak PM Peak Off Peak | 5 2 5 0 | 0 0 12 0 | 5 2 -7 0 |
| | WB | AM Peak Noon Peak PM Peak Off Peak | 2 1 2 0 | 0 1 1 0 | 2 0 1 0 |

$$n = 8$$
 $\bar{D} = 0.375$

$$S_{\overline{d}} = 1.21$$

t = 0.310

$$t_{.05}(7d.f.) = 1.895$$

 $^{\circ}_{\bullet}$ Accept H_{O} , Reject H_{A}

TABLE H.3

| STREET | DIRECTION | PERIOD | STOPS BEFORE (B) | STOPS AFTER (A) | DIFFERENCE B - A (D) |
|------------|-----------|---|------------------------|-----------------------|----------------------------|
| Adams | NB | AM Peak Noon Peak PM Peak | 7 9 10 | 1 5 19 | 6 4 - 9 |
| | SB | AM Peak Noon Peak PM Peak Off Peak | 6 9 9 10 | 0 13 8 12 | 6 -4 1 -2 |
| Washington | NB | AM Peak Noon Peak PM Peak Off Peak | 4 6 11 1 | 5 2 11 0 | -1 4 0 1 |
| | SB | AM Peak Noon Peak PM Peak Off Peak | 0 2 1 1 | 3 0 0 0 | -3 2 1 1 |

TABLE H.4

| STREET | DIRECTION | PERIOD | STOPS BEFORE (B) | STOPS AFTER (A) | DIFFERENCE B - A (D) |
|---------|-----------|---|------------------------|-----------------------|----------------------------|
| Georgia | NB | AM Peak Noon Peak PM Peak Off Peak | 15 20 17 15 | 0 13 14 0 | 15 7 3 15 |
| | SB | AM Peak Noon Peak PM Peak Off Peak | 9 14 14 10 | 2 1 5 5 | 7 13 9 5 |

$$n = 8$$
 $\bar{D} = 9.25$

$$S_{\overline{d}} = 1.62$$

$$t_{.05}(7d.f.) = 1.895$$

$$t_{calc.} = 5.70 > 1.895$$
, . Reject H_0 , Accept H_A

TABLE H.5

| STREET | DIRECTION | PERIOD | STOPS BEFORE (B) | STOPS AFTER (A) | DIFFERENCE B - A (D) |
|---------|-----------|--------------------------------|------------------------|-----------------------|----------------------------|
| Western | NB | AM Peak PM Peak Off Peak | 5 2 4 | 0 4 6 | 5 -2 -2 |
| | SB | AM Peak PM Peak Off Peak | 4 5 2 | 0 5 1 | 4 0 1 |

$$S_{\overline{d}} = 1.21$$

$$\bar{D} = 1.0$$

$$t = 0.83$$

$$t_{.05}$$
5d.f.) = 2.015

APPENDIX I

CALCULATION OF VEHICLE OPERATING COSTS

The annual operating cost during the before and after period would be computed as follows:

Annual Operating Cost = Cost of Stops + Excess Idling Cost +
Motorist' Excess Time Costs =

$$(\frac{\text{Stops}}{\text{Day}})$$
 (365) $(\frac{\text{Cost}}{\text{Stop}}) + (\frac{\text{Veh-Hr}}{\text{Day}})$ (365) $(\frac{\text{Cost}}{\text{Veh-Hr}}) + (\frac{\text{Veh-Hr}}{\text{Day}})$ (365) $(\frac{\$}{\text{Hour}})$

Using this method of analysis the excess motorists' operating cost (above the constant speed cost) in the before period is as follows:

$$C_{B} = \frac{(354,084\frac{\text{Stops}}{\text{Day}})365\frac{\text{Days}}{\text{Year}})(6.96)(.9)}{1000} + \frac{(354,084)(365)(58.85)(.1)}{1000} + \frac{(1664.8)(365)(114.86)(.9)}{1000} + \frac{(1664.8)(365)(225)(.1)}{1000} + \frac{(1664.8\frac{\text{Veh-Hr}}{\text{Day}})(365\frac{\text{Days}}{\text{Year}})($1/\text{vehicle-hour})}{C_{B}} = 809,563 + 760,581 + 62,815 + 13,672 + 607,652$$

$$C_{B} = $2,254,283$$

In a similar manner the motorists' operating cost after installation of the computer controlled signal system is computed.

$$C_{A} = \frac{(271,978)(365)(6.96)(.9)}{1000} + \frac{(271,978)(365)(58.85)(.1)}{1000} + \frac{(1019.1)(365)(114.86)(.9)}{1000} + \frac{(1019.1)(365)(225)(.1)}{1000} + (1019.1)(365)($1/vehicle-hour)$$

$$C_{\Lambda} = 621,840 + 584,216 + 38,452 + 371,972$$

$$C_{\Delta} = $1,624,849$$

Annual Reduction in Motorists Operating Cost =

$$$2,254,283 - $1,624,849 = $629,434$$

The equivalent uniform annual cost for the installation assuming a 10 year life and an interest rate of 8% is

$$EUAC = (\$1,958,000)(CRF-8\% - 10 yrs)$$

$$EUAC = (\$1,958,000)(0.149029)$$

EUAC = \$291,800

Assuming the cost and expected life of the components to be

| Item | Cost | <u>Life</u> |
|-----------------------------------|-----------|-------------|
| Conduit and Cable | 1,250,000 | 30 years |
| Poles, Heads and Controllers | 450,000 | 20 years |
| Computer and Peripheral Equipment | 250,000 | 10 years |

$$EUAC = $111,034 + 45,833 + 37,257$$

$$EUAC = $194,124$$

$$C_{B} = \frac{(354,084 \frac{\text{Stops}}{\text{Day}})(365 \frac{\text{Days}}{\text{Year}})(11.25 \frac{\$}{1000 \text{ Stops}})(.9) + }{1000}$$

$$\frac{(354,084)(365)(58.77)(.1)}{1000} +$$

$$\frac{(1664\frac{\text{Veh-Hr}}{\text{Day}})(365\frac{\text{Days}}{\text{Year}})(312.64\frac{\$}{1000 \text{ hrs.}})(.9)}{1000} +$$

 $r = (\frac{.020927}{.04339}) (.05) + .25$

APPENDIX J

FUEL CONSUMPTION REDUCTION WORKSHEET

Reduced vehicle-hour delay per year (idling):

$$(645.7 \frac{\text{vehicle-hour}}{\text{day}}) (365 \frac{\text{day}}{\text{year}}) = 235,681$$

2. Gallons consumed per vehicle-hour delay (idling):

0.58

3. Total gallons saved by reduction of delay/year (1 \times 2):

136,695

4. Reduced vehicle stops per year:

$$(82,106 \frac{\text{stops}}{\text{day}}) (365) = 29,968,690$$

5. Gallons consumed per vehicle-stop:

0.01

6. Total gallons saved per year by reduction of vehicle-stops (4 \times 5):

299,687

7. Total fuel saved per year, gallons (3 + 6):

436,382 gallons

APPENDIX K

AIR POLLUTION REDUCTION WORKSHEET

1. Reduced Vehicle-Hours Delay Per Year (Idling)

$$(645.7 \frac{\text{vehicle-hour}}{\text{day}}) (365 \frac{\text{day}}{\text{year}}) = 235,681$$

2. Reduced Annual HC emissions from idling (1. x .0087 $\frac{1bs.}{hr}$)

235,681 hr. of idling (.0087
$$\frac{1bs}{hr}$$
) = 2050 lbs.

3. Reduced HC emissions from reduced stops (from 25 mph)

(29,967
$$\frac{\text{thousand-stops}}{\text{yr.}}$$
) (.01 $\frac{\text{lbs.}}{\text{thousand-stops}}$) =

$$(300 \frac{1bs}{yr})$$
 HC Reduction

4. Reduced CO emissions from reduction in idling

(Reduction in idling) (CO emissions in $\frac{1bs.}{vehicle-hour}$)

$$(235,681 \frac{\text{vehicle-hour}}{\text{year}}) (1.19 \frac{\text{lbs.}}{\text{vehicle-hour}}) = 280,460 \frac{\text{lbs.}}{\text{yr}}$$

5. Reduced CO emission from reduction in stops

$$(29,967 \frac{\text{thousand-stops}}{\text{year}}) (10 \frac{\text{lbs.}}{\text{thousand-stops}}) = 299,670 \frac{\text{lbs.}}{\text{yr}}$$

Total Reduction From Project:

HC:
$$2350 \frac{1bs.}{year}$$

Co: 580,130
$$\frac{1bs.}{year}$$